Research Repo.

Physiological System Integrations with Emphasis on the Respiratory - Cardiovascular System

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PHYSIOLOGICAL SYSTEM INTEGRATIONS WITH EMPHASIS ON THE RESPIRATORY-CARDIOVASCULAR SYSTEM

TABLE OF CONTENTS

I.	Introduction	Page 1
2.	Overall Integrated Simulation	2
3.	Initialization and Reinitialization Interface	4
	 3.1 Circulatory to Cardiovascular 3.2 Circulatory to Thermoregulatory 3.3 Circulatory to Respiratory 3.4 Short-term to Long-term Transfer of Information 	4 4 4 5
4.	Short-term Model Interfaces	6
	 4.1 Respiratory-Thermoregulatory System Interface 4.2 Cardiovascular-Thermoregulatroy System Interface 4.3 Respiratory-Cardiovascular System Interface 	6 6 7
5.	Modifications of Individual Respiratory System	·11
6.	Evaluation of Integrated Respiratory-Cardiovascular System	13
7.	Appendix	26
	7.1 Program Listing of Particular Subroutines	26
8.	Bibliography	62

1. INTRODUCTION

This report deals with the integration of two types of physiological system simulations. These types are classified as long-term and short-term. The long-term model is a circulatory system model which simulates long-term blood flow variations and compartmental fluid shifts. (1) The short-term models simulate transient phenomena of the respiratory, thermoregulatory, and pulsatile cardiovascular systems as they respond to stimuli such as LBNP, exercise, and environmental gaseous variations. (2-4) An overview of the interfacing approach is described in Section 2. Detailed descriptions of the variable interface for long-term to short-term and between the three short-term models are given in succeeding sections of this report.

In order to fulfill the objectives of the study each system was carefully analyzed. Types of inputs and simulation forcing functions were evaluated. When an identical physiological variable was calculated by more than one model, the calculation which was most physiologically based was retained as an interfacing variable.

The major emphasis of this component of the study concentrated on the respiratory-pulsatile cardiovascular system with exercise playing the role of a major stimulus. Studies of simulations involving this integrated system and its response to altered environmental gaseous concentrations (0₂, CO₂) are being conducted.

2. OVERALL INTEGRATED SIMULATION

For implementation of the simulation of an experiment which might encompass hours, days, and even weeks it is mandatory that two interfacing segments be considered. One of these would handle the transfer of variable and parameter values during short-term simulations when all short-term transient models are functioning. The other interface would allow transfer of information in an initialization or reinitialization mode. These two interfacing segments are illustrated in Figure 1. The interface between the short-term transient models and the long-term model is also utilized as the input for the experimental protocol.

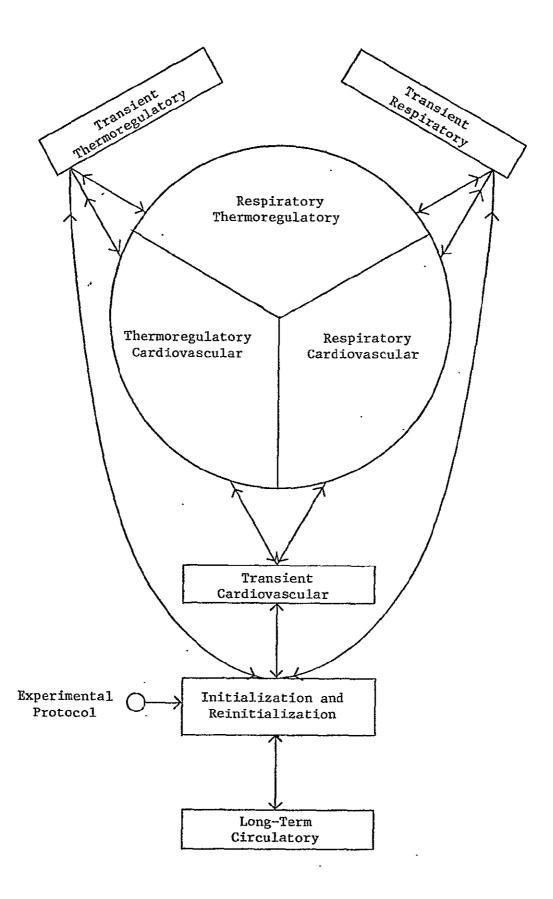


Figure 1. Overall interfacing schemes of transient and long-term physiological system models.

3. INITIALIZATION AND REINITIALIZATION INTERFACE

In the following Sections brief descriptions of the salient interfacing features are presented. Since the interface is not individualized with regard to specific system types, much of the initialization of variables is common to all the systems.

3.1 Circulatory to Cardiovascular

Establishment of blood volumes after long-term simulations is important. In particular, the unstressed volume (V_0) reflecting shifts due to antonomic stimulation needs to be transferred along with total blood volume. Changes in the resistance flow segments, such as in the renal component, play important roles in transient simulations of exercise. Whether implemented as alterations in peripheral resistance or by some other mechanism a cardiac output influence is necessary.

3.2 Circulatory to Thermoregulatory

Skin blood flow is a variable that contributes to the particular compartmentalization of the thermoregulatory system, thus it is necessary that long-term shifts in this variable be realized. No other variables are strictly inherent between these two systems. That is, other thermoregulatory system variables are available for reinitialization through the cardiovascular and respiratory system components.

3.3 Circulatory to Respiratory

A cardiac output update is obtained from the circulatory system via the cardiovascular system. This transfer of variable seems logical since the cardiac output component is removed from the respiratory system and total blood flow is generated for all three short-term models by the cardiovascular system. Long-term changes in metabolic rates must be transferred to the respiratory system. In addition, the blood hemoglobin (Hb) level variations are necessary for establishing arterial hemoglobin concentrations ($Ca_{(HbO_2)}$) in the respiratory system.

3.4 Short-term to Long-term Transfer of Information

Necessary initialization data from the thermoregulatory system include skin blood flow and a water loss variable. Skin blood flow reflects the short-term thermal environmental changes as well as related physiological changes. Since the long-term circulatory system model does not formulate evaporative loss, the evaporative water loss from the thermoregulatory system would be utilized as an increased water loss. Consequently, the circulatory system would not further distinguish the total water loss and the evaporative loss. Details of these variable flows will be pursued in a future study.

Presently, the significant variable transfer from the respiratory to circulatory system is the variation in $\text{Ca}_{(\text{HbO}_2)}$. The cardiac output influence is the dominant contributor from the cardiovascular to circulatory system. As the integrated system is further developed and refined, it is likely that other variables will be added to this initialization and reinitialization component.

4. SHORT-TERM MODEL INTERFACES

In the top portion of Figure 1 the short-term model interfaces are displayed. A closer look at the particular variables involved is given here. Greater emphasis is placed upon the respiratory-cardiovascular system interface since the immediate study concentrates on this phase.

4.1 Respiratory-Thermoregulatory System Interface

Only the variable which describes respiratory minute volume is directly transferred to the thermoregulatory system. It is an input used in describing water loss and heat loss formulation. Other variables of the thermoregulatory system which are influenced by the respiratory system are transferred by the cardiovascular system. These include cerebral blood flow and metabolic rates. No variables are passed directly from the thermoregulatory to the respiratory system.

4.2 Cardiovascular-Thermoregulatory System Interface

There are several variables passed from the cardiovascular to the thermoregulatory system. Blood flows including total cardiac output, muscle blood flow due to exercise, and cerebral blood flow are passed to the thermoregulatroy system. It should be noted that the cerebral blood flow formulation originates in the respiratory system. In a similar manner metabolic rates are transferred to the thermoregulatory system via the cardiovascular system. Body attitude (standing, sitting, prone) as it relates to shunted blood flow due to physiological stress and peripheral resistance is transferred in a manner useful to the thermoregulatory system.

The reverse transfer of information yields skin blood flow, a cardiac output influence, and a blood shunting influence due to thermal environmental

contributions. These are then used to update or augment existing formulations in the cardiovascular system.

4.3 Respiratory-Cardiovascular System Interface

Cerebral blood flow, described as a function of arterial ${\rm CO}_2$ and ${\rm O}_2$ gas tensions in the respiratory system is passed to the cardiovascular system. The variable, respiratory frequency, is transferred to the cardiovascular system. Refer to Section 5 for a description of the modified version of this expression. Instead of passing an a-v ${\rm O}_2$ difference term and having total oxygen uptake calculated in the cardiovascular system, the entire development of oxygen demand is retained in the respiratory system. Oxygen demand is then passed to the cardiovascular system. Although not completely developed, arterial ${\rm CO}_2$ and ${\rm O}_2$ tensions are passed to the cardiovascular system with the idea that they will be utilized in an implementation of ${\rm CO}_2$ and ${\rm O}_2$ forcing for a cardiac output formulation.

In order to fulfill the demands of the forementioned mechanism, the resting O₂ requirement (VO2RDT) and total metabolic rate (VO2DT) for a given exercise level is transferred to the respiratory system. The cardiac output subroutine is deleted from the respiratory system with cardiac output requirements fulfilled by a transfer from the cardiovascular system.

Interface modifications are established in the following manner. The block diagram for controlling metabolic rate which existed in the cardio-vascular system is modified to the one which appears in Figure 2. A common interface has been established as

COMMON/RINTR/ROUT(10), CIN(10).

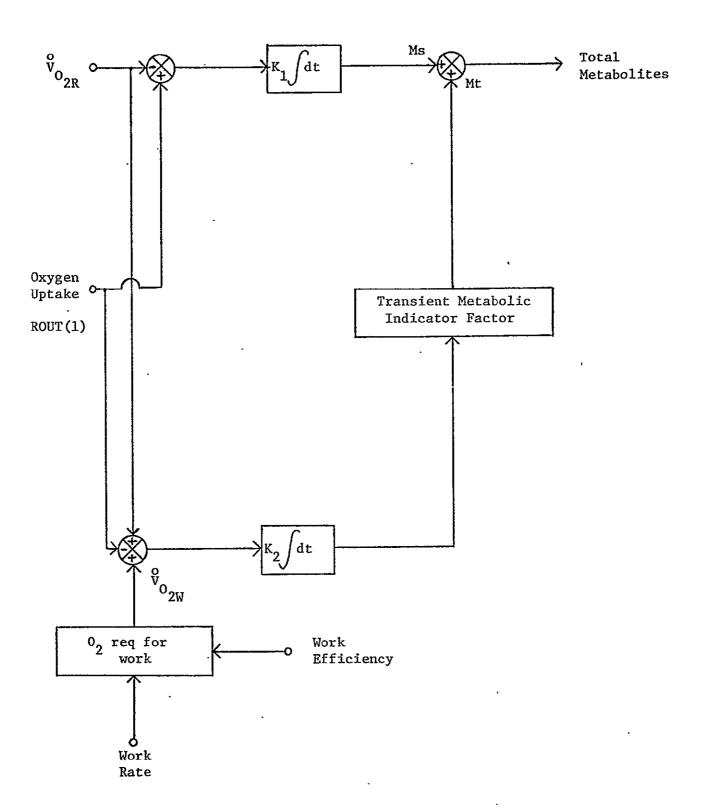


Figure 2. Revised block diagram for controlling metabolic rate in the cardiovascular system. Variable ROUT(1) is obtained from the respiratory system.

In the respiratory model, Subroutine RC12, the output variables are indicated as

```
ROUT(1) = AVO2DM/1000

ROUT(2) = FREQ

ROUT(3) = C(11)

ROUT(4) = F(7)

ROUT(5) = F(1) (4.1)
```

where

```
AVO2DM = a-v 0<sub>2</sub> difference, ml0<sub>2</sub>/min,

FREQ = respiratory frequency, bpm,

C(11) = cerebral blood flow, 1/min,

F(7) = Pa(CO<sub>2</sub>), mmHg, and

F(1) = Pa(O<sub>2</sub>), mmHg.
```

Likewise, the input variables are indicated as

```
C(10) = CIN(1)

VO2DT = CIN(2)

VO2RDT = CIN(3) (4.2)
```

where

```
C(10) = cardiac output, 1/min, VO2DT = oxygen required for particular work load, 10_2/\text{min}, and VO2RDT = oxygen required for resting state, 10_2/\text{min}.
```

In the SSO2W(X) Subroutine of the respiratory system, the following modification has been performed. The former subroutine statements were replaced by

```
COMMON/RINTR/ROUT(10), CIN(10)

VO2RDT = CIN(3) (4.3)

SSO2W(X) = VO2RDT - .0500 + (.0004850815 * 6.12 * X)/.25 (4.4)
```

where X = work load in watts and the other terms are as previously defined.

In Subroutine RC12 the following statements were added such that they appear in both the increasing and decreasing work load paths.

```
IF (WORK.LE.O.O .AND. NWREST.LT.1) RMT(2) = CIN(3)-C(26) AVO2DM = (F(9)*C(10)-F(13)*(C(10)-C(11))-F(12)*C(11))*1000. AVO2DF = AVO2DM/C(10) ROUT(1) = AVO2DM/1000. IF(WORK.GT.O.O) ROUT(1) = RMT(2)+C(26)
```

ROUT(2) = FREQ ROUT(3) = C(11) ROUT(4) = F(7) ROUT(5) = F(1)

The transfer of cardiac output from the cardiovascular to the respiratory system was handled in the main program, GRODIN, C(10) = CIN(1). Additions to COMMON/R/ in RC 12 include RMTM and TCT.

Refer to Appendix 7.1 for the program listing illustrating the implementation of these statements in Section 4.3 and the corresponding changes in the cardiovascular system.

5. MODIFICATION OF INDIVIDUAL RESPIRATORY SYSTEM

Improvement in the individual respiratory model was suggested in a previous research report. (5) These modifications were made and presently exist in the latest version of the respiratory system model. (6) In addition, a-v 02 difference (AVO2DF) and dead space volume (DSVOL) have been added to the output routines.

These modifications are summarized here. In the original model respiratory frequency (FREQ) was given by

$$FREQ = 8.1 + 7.815 * (RMT(2) + C(26))$$
 (5.1)

with

RMT(2) = 0 metabolic rate of tissue and

C(26) = 0, metabolic rate of brain.

Thus, Equation 5.1 didn't respond to any forcing other than $\mathbf{0}_2$ demand. This formulation was replaced by

FREQ =
$$\frac{\left(\left(1 + 32 \left(\frac{1 + a}{a}\right) RC \right)^{2} V_{A}}{16\left(\frac{1 + a}{a}\right) RC} - 1\right)}{16\left(\frac{1 + a}{a}\right) RC}$$
 (5.2)

with

 $RC = 0.015 \min$

 $\overset{\text{o}}{V}_{\Delta} \approx V_{E} = \text{expired ventilation},$

a = 1.95 =
$$\frac{\text{inspiratory elastance}}{\text{expiratory elastance}} = \frac{K_{T}}{K_{E}}$$
 , and

DSVOL = dead space volume, (5)

Upon substituting the constants, FREQ is given by

$$FREQ = ((1. + (.726 * VE)/DSVOL)**.5 - 1.)/.363$$
 (5.3)

with

$$DSVOL = 0.140 + 0.002 * VE$$
 (5.4)

Dead space ventilation, originally defined as

$$DEADVT = .1107 * FREQ + .0785 * VE$$
 (5.5)

is now given by

DEADVT =
$$1 + .098 * VE$$
. (5.6)

The representation for minute volume (TVNT) remains unchanged.

The a-v 0_2 difference expression that is necessary for the integrated system to function is added to RC12. Here,

$$AVO2DF = AVO2DM/C(10)$$
 (5.7)

where

C(10) = cardiac output and

AVO2DM = (F(9) * C(10) - F(13) * (C(10) - C(11)) - F(12) * C(11)) * 1000as defined in Section 4.

The terms in AVO2DM are defined in exactly the same way as in the original respiratory system model. See Appendix D of the listed reference. (7) Also, in comparison of the original respiratory program and the latest modified version there are additions to the output statements of RC12.(5-7) Statement #'s 218, 219, and 220 have been modified to include AVO2DF and DSVOL. In a similar manner statement #'s 246, 263, 264, and 265 now include these new output variables.

Before leaving the discussion of the calculation of a-v O₂ difference the significance of transport delays should be considered. Slight errors exist in the present formulation. Blood flow transport delay times are not considered in the calculation of venous blood concentrations. See Equation 5.7. Actually the concentrations and compartmental blood flows should correspond to the same time. This means that an additional book-keeping operation should be implemented such that the concentration at the lung entrance reflects the delay times and their corresponding contributions.

6. EVALUATION OF INTEGRATED RESPIRATORY-CARDIOVASCULAR SYSTEM

The evaluation of the integrated respiratory-cardiovascular system proved quite encouraging. Several types of simulations were tried. A 200-watt exercise level of 5 minute duration was used as the stimulus. In this section two systems are compared. The basic difference between the two systems involves the formulation of metabolic requirements. System A is shown in Figure 3 and System B is shown in Figure 4. Selected responses for these two systems are illustrated in Figures 5-14.

The major variations in the responses can be summarized as follows. System B doesn't allow for the rapid increase in heart rate that occurs with System A. Since the cardiac output doesn't vary appreciably between the two systems, the over response in heart rate of System A is accompanied by a decrease in stroke volume. System B is a slightly more efficient system since a lesser amount of 0_2 (0.1 10_2 /min) is required to sustain the simulation at this steady-state exercise level. The differences in the pre-exercise variable levels are related to the differences of basal conditions for the respiratory system and resting conditions for the cardiac output system. This feature is coupled with the fact that the cardiac output settles to ≈ 6.8 1/min compared to the 6 1/min for the original respiratory system. After considering all of the variables' responses and the control of regulation involved with each one, System B seems to perform in a more satisfying manner. Therefore, the system shown in Figure 4 is recommended as the integrated system for exercise simulations.

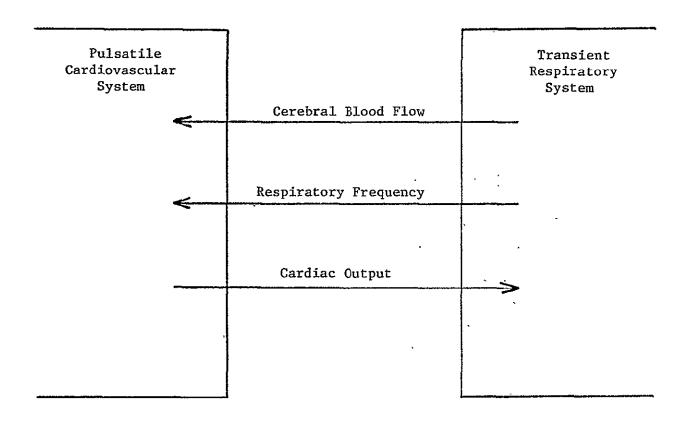


Figure 3. Respiratory-cardiovascular system interface which retains the metabolic formulation in each model during exercise stimulation

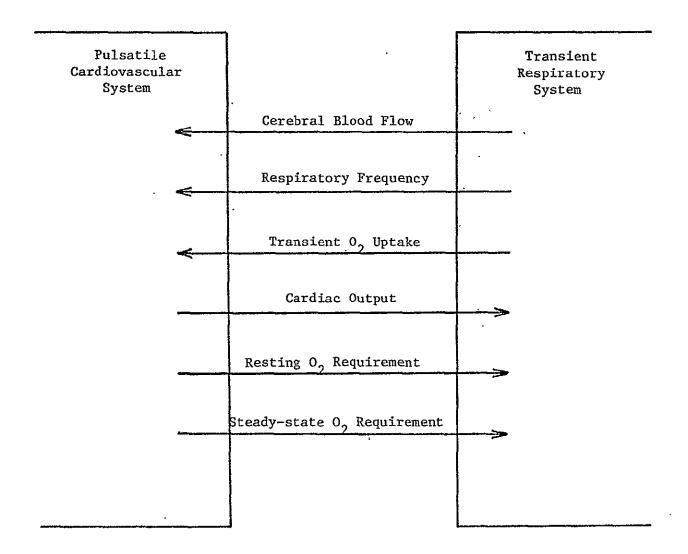


Figure 4. Respiratory-cardiovascular system interface which utilizes the metabolic formulation of the respiratory system during exercise stimulation.

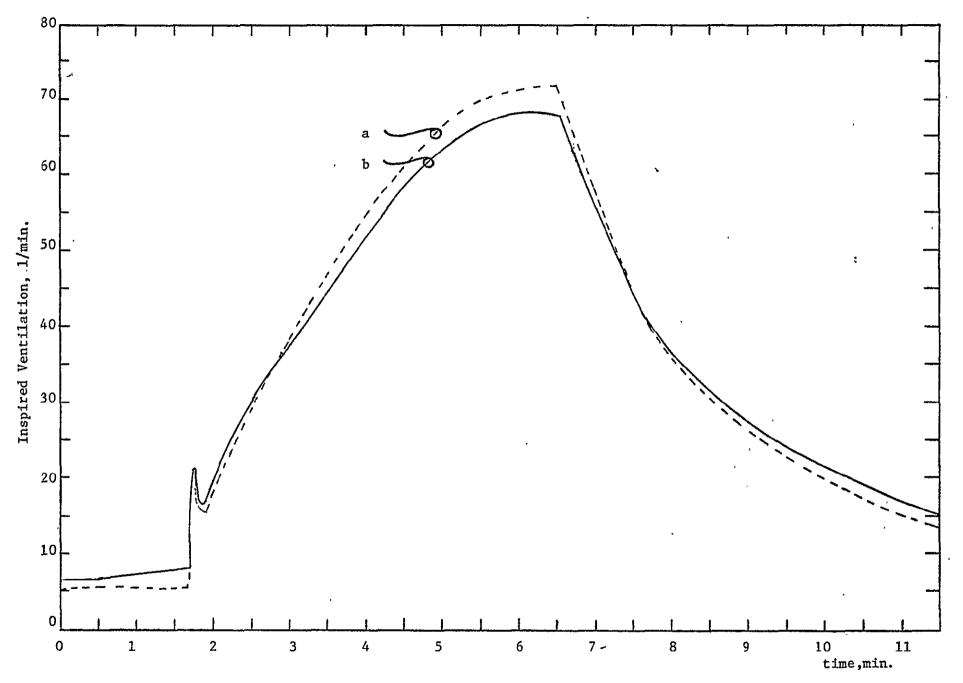


Figure 5. Inspired ventilation versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

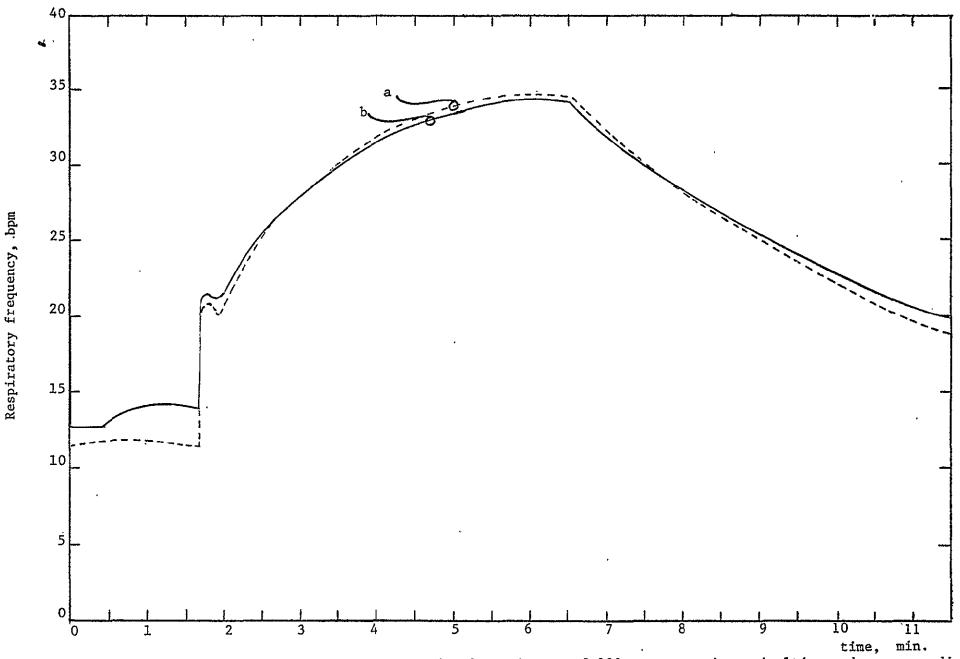


Figure 6. Respiratory frequency versus time for five minutes of 200 watt exercise stimultion and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

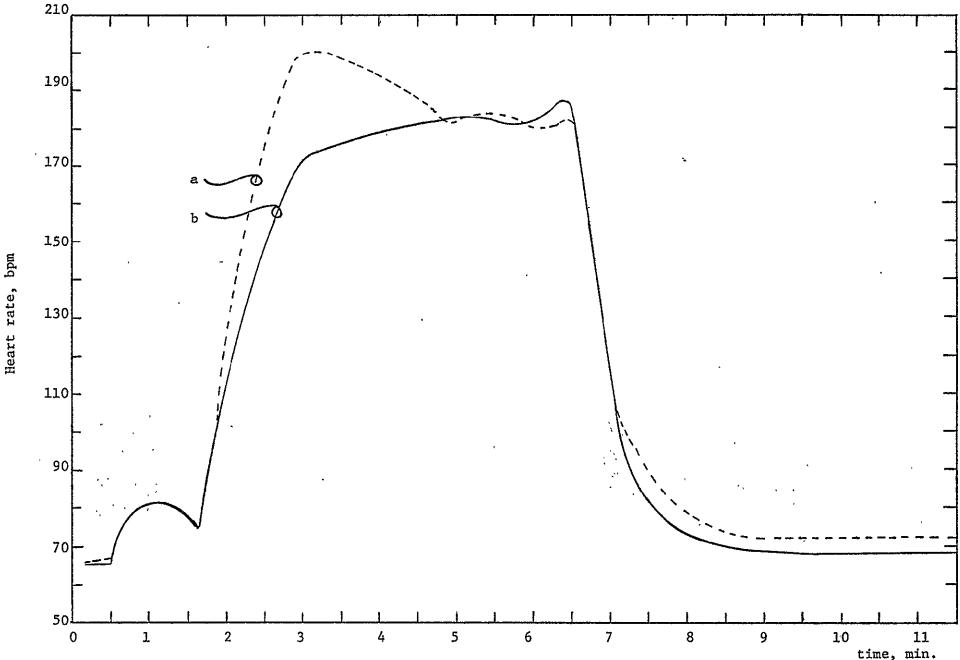


Figure 7. Heart rate versus time for five minutes of 200 watt exercise stimulation and corresponding offtransient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

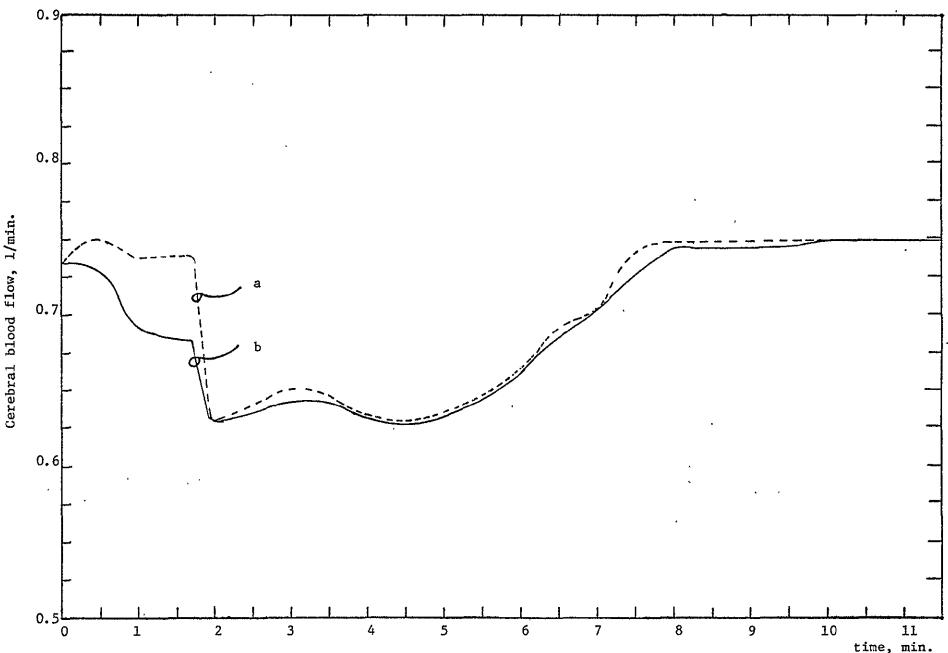


Figure 8. Cerebral blood flow versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

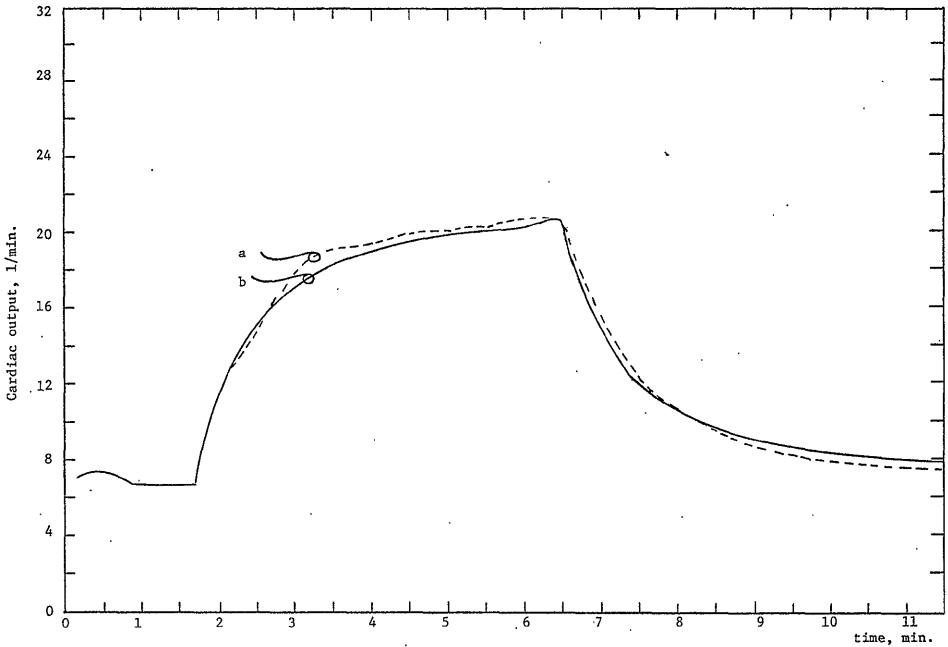


Figure 9. Cardiac output versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model

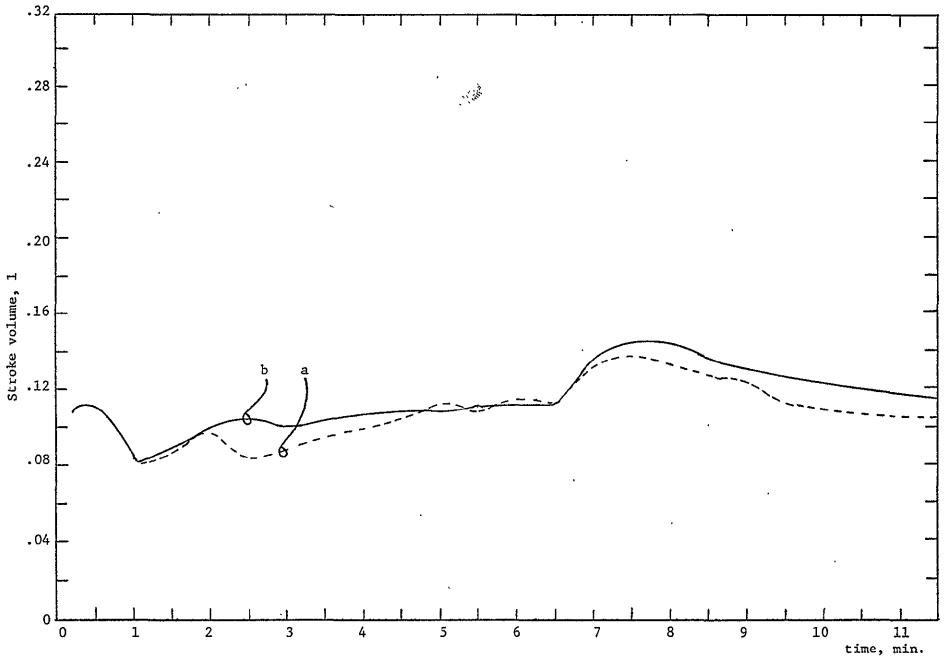


Figure 10. Stroke volume versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

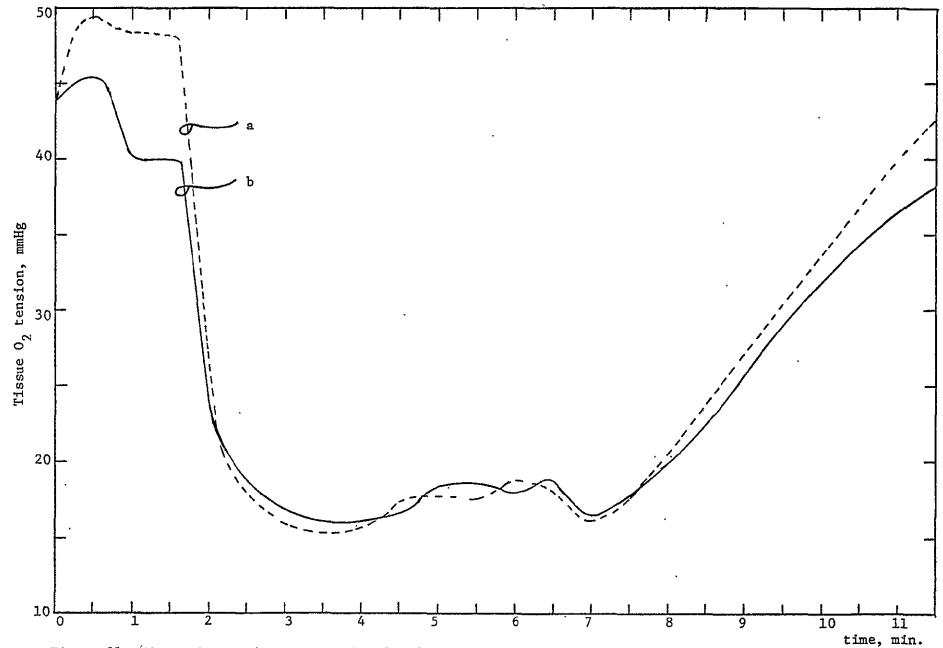


Figure 11. Tissue 0₂ tension versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model

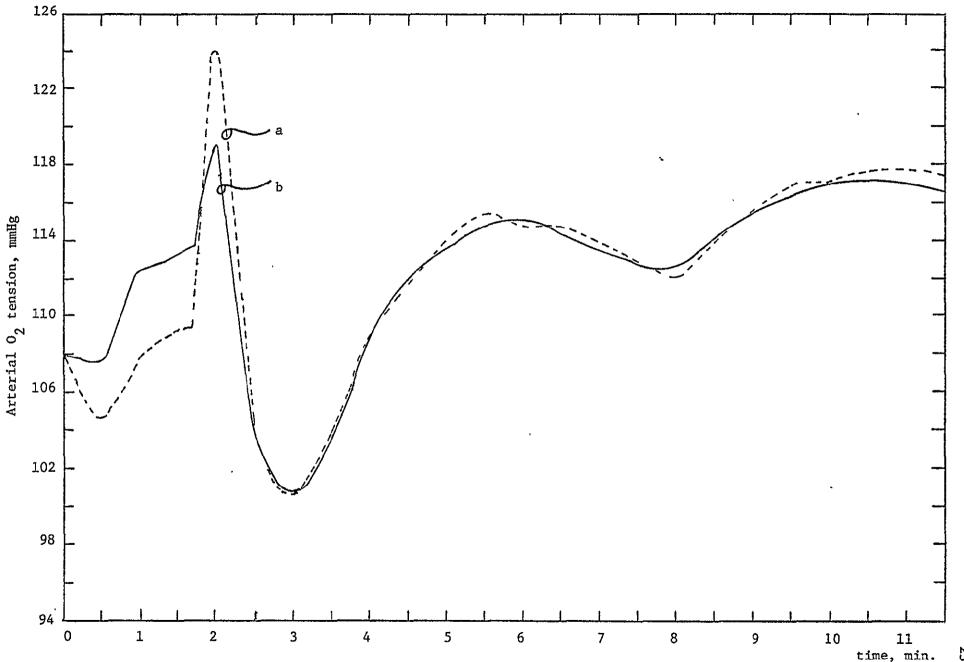


Figure 12. Arterial 0₂ tension versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

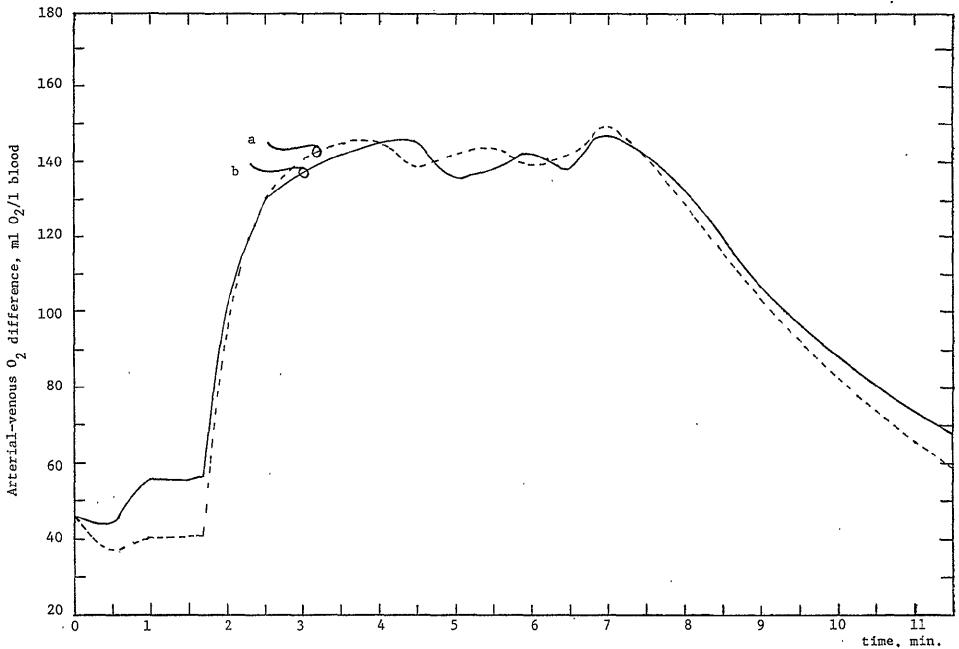


Figure 13. Arterial-venous 0 difference versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

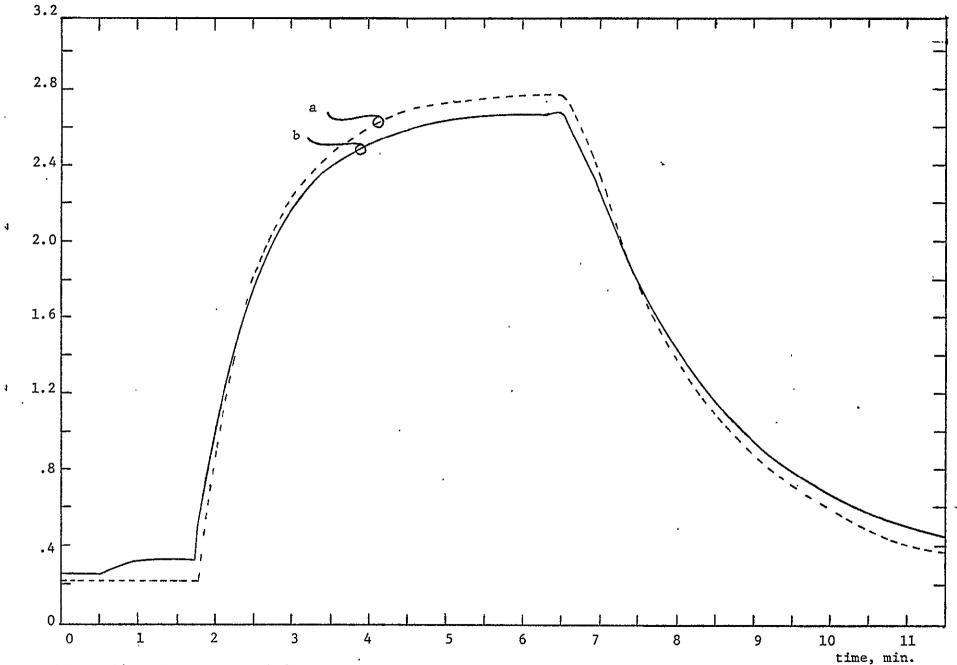


Figure 14. Tissue 0, metabolic rate versus time for five minutes of 200 watt exercise stimulation and corresponding off-transient response. (a) Individual cardiovascular and respiratory system simulations of metabolic requirements. (b) Metabolic requirements controlled by respiratory system model.

7. APPENDIX

7.1 Program Listing of Particular Subroutines

Computer 'Program Listing of the subroutines of the respiratory system and pulsatile cardiovascular system models which were modified for the integration of the two systems.

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-37		C - BLOOD DXYGEN CAPACITY "	
38	(C 17 (Ha)	•
39	(C TIME CONSTANTS IN CARDIAC OUTPUT AND CEREBRAL BLOOD FLOW RESPONSES.	
40	9	C 18 R1 C 19 R2	
41 - 42		C 19 R2	
	`	CCONTROLLER EQUATION SENSITIVITY WEIGHTINGS.	
44	č	C 20 CENTRAL SENSITIVITY COEFFICIENT .	
45.	· - č	C - 21 CAROTIO BODY SENSITIVITY COEFFICIENT.	
46	•	c	
47	•	C VOLUMES OF LUNG. SRAIN. AND TISSUE	
48		C 22 KL	
49—	<u></u> -	C 24 Vr	
50 51 -		C 24 KT C - · · · · · · · · · · · · · · · · · ·	
52		C BRAIN METABOLIC RATE OF CO2 PRODUCTION.	
53		C 25 HRA(CO2)	
54	Č	C BRAIN METABOLIC RATE OF 02 CONSUMPTION.	-

				<u>.</u>
57	C 27 DCn2		•	۶ -
58	C 28 · DO2 ·		** ** *********************************	
59 •	C 29 DN2		•	
	s		 	^ 3
61	6 BAROMETRIC PRESSURE.		•	:
7. -	C 30 B			
	C VOL*FRACTION OF INSPIRED GAS. C·· 31F1(CO2)			
65	C 32 F1(02)			π
	C · 33 FI(N2)			
67				
6B	C VOL.OF CSF			
69	C 34 KCSF			
	C-INITIAL TIME			_
	C 35 T			
	C. COMPUTER TIME STEP	-		-•
73	C 36 H	380AV.401.		
	C CONTROLLER EQUATION CONSTANT(MAINTAINS RESTING PA(COZ) AF	1 100, 40, 40, 40, 40, 40, 40, 40, 40, 40,		-
	C- VALUE-FOR RESTING AL-VENTILATION		· · · · · · · · · · · · · · · · · · ·	
77	C 38 VI(SS)			
	C OUTPUT PRINT INCREMENTS (ALSO PRINTS AT +5MIN+INCRIMENTS)	;•	, a see see value and the see see see see see see see see see s	
79	C 39 PRINT-ALL TIME		•	
ao -	C no e	3 3 * 4 * **		
81	C SV(18.50)	ı	,	
82	CARTERIAL GAS CONCENTRATIONS AT LUNG EXIT+			_
8.3	C 1 CA(CO2)			
84	C	• •		-
	C	<u> </u>	_ H Ž	_
	C VENOUS GAS CONCENTRATIONS AT BRAIN EXIT.	•	™ 📆	
aa	C 4 - CV8(CO2)		<u> </u>	
89	C 5 CVA(02)		<u>o</u> <u>e</u>	
	C 6 CV8(N2)		·	
91	C . Weno to the squashyour land of Tische Cyll.		· 27	
93	C YENOUS GAS CONCENTRATIONS-AT TISSUE EXIT	/* ****	58	
94	C 8- CVT(02)		JAL	
95	C 9 CVT(N2)	• "	-	
96	C		. * 9	_
·97	C CARDIAC OUTPUT.			
	6 (10 0)			
	C CEREBRAL BLOOD FLOH.		•	
101	C-			
10Z				_
103	C ARTERIAL H+ CONCENTRATION.			_
	C 13 CA(H+)		·	_
105	C ARTERIAL OZ TENSION.		•	
106				
107	<u>c</u>			
108	C 15 C TOTAL GAS CONCENTRATIONS AT BRAIN EXIT.			_
109	C			
	C TOTAL GAS CONCENTRATIONS AT TISSUE EXIT.	1		-
	G		. ΄ <u>, </u>	_
	C TIME.			
·				

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		· · · · · · · · · · · · · · · · · · ·	_
	-		
1 1 11	_	13 #	•
114	Ç	ia t	
	C	The state of the s	
116	c	VTRAN(18)	•
		ARTERIAL GAS CONCENTRATIONS AT BRAIN ENTRANCE.	
	4		
118	Ç	1 CAB(CO2) * CA(CO2)(T - TAB) /	
119	- ··· c · ·	2 CAB(02) # CA(02) T = TAB)	
120		3 CABINZ) = CAINZ) IT - TAB	
	<u>C</u>	CABANA CAMBANA (ABA	
121	ç-		
122	Ç	VENOUS BRAIN GAS CONCENTRATION AT LUNG ENTRANCE.	
123			
124	Ž	5 CV8(02)(T - TV8)	
125	, C	6 CVB(N2)(T = TV8)	
126	c	_	
127		VENOUS TISSUE GAS CONCENTRATION AT LUNG-ENTRANCES	
128		7 CVT(C02)(T - TVT)	
	•		
129	· · ·- C - ·	8 CVT(02)(T - TVT)	
130	c	9 CVT(N2)(T - TVT)	
131	<u>:</u> .		
131	č	ADTOCAL C.C. CAMPENTOATIANS AT TIRCUIS ENTRANCE	
-	Ç	ARTERIAL GAS CONCENTRATIONS AT TISSUE ENTRANCE.	
133		10 CAT(CO2) = CA(CO2)(T'- TAT)	_
134	c	11 CAT(02) = CA(02)(T - TAT)	<u>.</u>
	-	12 CAT(N2) = CA(N2)(T - TAT)	
	_	1- 64(102) - 64(10-7) - 74(1	,
136	C		•
13,7	· - c -	ARTERIAL H+ CONCENTRATION AT CAROTIO BODIES'SITE	
138	c	13 CAO(H+) = CA(H+)(T - TAO)	
	.	•	
139		ARTERIAL 02 TENSION AT CAROTIO BODIES*SITE.	
140	C	14 PAO(O2) = PA(O2)(T - TAO)	
141	· - c	ARTERIAL H+ CONCENTRATION AT BRAIN ENTRANCE.	
142	~		
		15 CAB(H+) = CA(H+)(T - TAB)	
- 143		TOTAL GAS CONCENTRATION FROM BRAIN AT LUNG ENTRANCE.	
- 143	c	TOTAL GAS CONCENTRATION FROM BRAIN AT LUNG ENTRANCE	
	c	16 (CA3(CO5) + CAB(U5) + CAB(N5))(L - 1AB)	OF RE
· 144 ——145 -	c	16 (CV3(CO2) + CV8(n2) + CV8(n2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE+	OF RE
. 144 	c	16 (CA3(CO5) + CAB(U5) + CAB(N5))(L - 1AB)	
· 144 ——145 -	c	16 (CV3(CO2) + CV8(n2) + CV8(n2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE+	
. 144 	c c 	16 (CV8(CO2) + CV8(Q2) + CV8(N2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM T15SUE AT LUNG ENTRANCE+	OF POOR
144 	c c 	16 (CV8(CO2) + CV8(Q2) + CV8(N2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM T15SUE AT LUNG ENTRANCE+	POOR .
144 		16 (CVB(CO2) + CVB(D2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE 17 (CVI(CO2) + CVI(D2) + CVI(N2))(T = TVI) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS	POOR .
144 		16 (CVB(CO2) + CVB(D2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVI(CD2) + CVI(D2) + CVI(N2))(T = TVI) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF-OF GASES,	POOR OU
144 		16 (CVB(CO2) + CVB(D2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE 17 (CVI(CO2) + CVI(D2) + CVI(N2))(T = TVI) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS	POOR OU
144 		16 (CVB(CO2) + CVB(D2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVI(CD2) + CVI(D2) + CVI(N2))(T = TVI) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF-OF GASES,	POOR .
144 		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF.OF GASES, -H=COMPUTER TIME-STEP. HB=BLOOD-OXYGEN-CAPACITY	GINAL PAGE
144 		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES, H=COMPUTER TIME-STEP, HB=BLOOD-OXYGEN-CAPACITY- 1 5 = 47 - 2 K ACO2	GINAL PAGE
144 		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES,	POOR OU
144 		16 (CVB(CO2) + CVB(D2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVI(CD2) + CVT(D2) + CVT(N2))(T = TVT) O(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF-OF GASES, H=COMPUTER TIME-STEP. HB=BLOOD OXYGEN-CAPACITY 1	GINAL PAGE
144 		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES,	GINAL PAGE
144 		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS. K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES,	GINAL PAGE
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144		16 (CV8(CO2) + CV8(D2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(D2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES, H=COMPUTER TIME-STEP. HB=BLOOD-OXYGEN-CAPACITY- 1	GINAL PAGE
144		16 (CVB(CO2) + CVB(N2) + CVB(N2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVI(CO2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF.OF GASES, -H=COMPUTER TIME-STEP. HB=BLOOD-OXYGEN-CAPACITY- 1	GINAL PAGE
144		16 (CV3(CO2) + CV8(O2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(O2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES,	GINAL PAGE
144		16 (CVB(CO2) + CVB(n2) + CVB(n2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVT(CD2) + CVT(n2) + CVT(n2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47=WATER VAPOR PRESS K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF=OF GASES,	GINAL PAGE
144		16 (CV3(CO2) + CV8(O2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(O2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF.OF GASES,	GINAL PAGE
144		16 (CVB(CO2) + CVB(n2) + CVB(n2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVT(CD2) + CVT(n2) + CVT(n2))(T = TVT) D(15) FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47=WATER VAPOR PRESS K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF=OF GASES,	GINAL PAGE
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144		16 (CV8(CO2) + CV8(O2) + CV8(N2))(T - TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(O2) + CVT(N2))(T - TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF+OF GASES,	GINAL PAGE
144 145 146 147 148		16 (CVB(CO2) + CVB(n2) + CVB(n2))(T = TVB) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CVI(CD2) + CVT(n2) + CVT(n2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF-OF GASES.	GINAL PAGE
144		16 (CV8(CO2) + CV8(O2) + CV8(N2))(T - TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(O2) + CVT(N2))(T - TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47*WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG, A=SOLUBILITY COEFF+OF GASES,	GINAL PAGE
144		16 (CV8(CO2) + CV8(Q2) + CV8(W2))(T = TV8) - TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CD2) + CVT(Q2) + CVT(W2))(T = TVT) O(15) - FOR D(15) THE SYMBOLS BEBAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF-OF GASES,	GINAL PAGE
144		16 (CV3(CO2) + CV8(Q2) + CV8(N2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE 17 (CV1(CO2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF.OF GASES, -H=COMPUTER TIME-STEP. HB=BLOOD OXYGEN-CAPACITY- 1	GINAL PAGE
144 145 146 147 148		16 (CV3(CO2) + CV8(Q2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(N2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF-OF GASES,	GINAL PAGE
144 145 146 147 148		16 (CV3(CO2) + CV8(Q2) + CV8(N2))(T = TV8) -TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE 17 (CV1(CO2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF.OF GASES, -H=COMPUTER TIME-STEP. HB=BLOOD OXYGEN-CAPACITY- 1	GINAL PAGE
144 145 146 147 148		16 (CV3(CO2) + CV8(Q2) + CV8(N2))(T = TV8) TOTAL-GAS CONCENTRATION FROM TISSUE AT LUNG ENTRANCE. 17 (CV1(CO2) + CVT(N2) + CVT(N2))(T = TVT) D(15) FOR D(15) THE SYMBOLS B=BAROMETRIC PRESSURE, 47=WATER VAPOR PRESS., K=CONVERSION FACTOR FOR ATM TO MMHG. A=SOLUBILITY COEFF-OF GASES,	GINAL PAGE

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3 PB(02)
                - -- 4 · K ACO2 PB(CO2)
   173
            c
                  5 PT(02)
  -174--
        --- C --- 6 . K ACO2 PT(CO2)
   175
                  7
                      PA(CO2)
-·- 176
                      PAIDZ
   177
                      CAIDZI
  -17A
              -- 10-
                     CA(N2) -- -- - . .
   179
                      CA(CUZ) + CA(UZ) + CA(NZ)
------
            C - " 12 · CVB(02) -- ·
   181
                 13 CVT(02)
------162
            C PRODUCT OF DIFFUSION COEFFS. AND GAS DIFFERENTIALS ACROSS BLOOD-BRAIN
   183
  -184
        · - -- C-BARRIER+-
                          . - -
                 14
                      DC02 (P8(C02) - PCSF(C02))
   185
            C
  186
          - C ---- 15
                      DO2 (P8(02) - PC5F(02))
   187
                 16
                      DN2 (PB(N2) - PCSF(N2))
  -188
                PB(02)
   189
            C
   -190
          191
                 DIMENSION XN8(4.2). 03(4). 103(2)
             -----COMMON/Z/ C. XN. SV. VTRAN. RK, SC. DC. A. D. F. VOL. RMT. BC. QF.
   192
   193
                      TAU, CC, CHB, CH, CPH, DQ, VE, VI, CPB, CPT, CADK, X, DT,
                       TIRK, LOC. ITERY, INDEX, I. J. M. N.
                 COMMONIAL XDS.XMH.CXT.VORK.DUMI.DUM2.DUM3.WORK2.RMTB.RMTB2.TIMEOF
   195
          ------ 1 .RMLIN.ITTY
---196
          C ITTY =FLG FOR TTY MODE.
   197
----- 198
          ---C--- O= OUTPUT TO PRINTER (BATCH MODE).
                 *TTY *= TTY I/O AND 19T TIME TO SUBROUTINE RC12.
         -- C -- 1 = TTY I/O AND NOT 1ST TIME TO KC12.
   231
                 DATA ITTTY/*ITY */
 --- 202 ------ C ----- DATA FOR INITIAL CONDITIONS
   233
                 C(IO)=CIN(I)
                                                                                               POOR
  - 204-
             - - IF (CXT.GT.D.) GO-TO AD
   205
                 #RITE (6.5)
        ----- 5 FORMAT (/* - GRODINS) RESPIRATORY CONTROL MODEL !//)
 -- 206
   207
            300 CONTINUE
 - 208--- -- - WRITE(6.483) · - --
   209
              483 FORMAT('DADD DATA...')
--- 210
         -- C-- READ INDICATION OF BATCH OR TTY HODE.
   211
                 READ(5.489) ITTY
  212
       -- - 480 FORMAT(A4)
                 IFILITY .NE. ITTIY) ITTY . ..
   213
  -214
             ----- #RITE(6.90) -- -
   215
               90 FORMAT (1H1,1X+37H+RESPIRATORY CHEMOSTAT -- INPUT DATA+/)
          -- C - DATA FOR INITIAL CONDITIONS
 216
   217
                  00 10 1 = 1,49
   218
            C 1106 HAS PROBLEM WITH ENDM , SO THIS ISNT USED TO
            C DETERMINE END OF RUN(NOO CAPABILITY TO START ANOTHER
   219
 -- 220.
           -E- . MODEL RUN IN SAME COMPUTER RUND.
   221
                 READ(5,190,EHD=301) C(1),(XN(1,J),J=1,2)
   222
               10 CONTINUE .
            C ESTABLISH COMPUTER STEP INDEPENDENT OF INPUT DATA.
   223
   224
                  C(36)=.78125E-2
   225
              190 FORMAT (5X,F15.0.54.244)
  - 226
           -- -- -- DO 20 I = 1.5
                 IP40 = I + 40
   227
```

	* ****		
228	READ (5,190) BC(1), (XNB(1,J), J = 1,2)		•
229			
230	00 30 1 = 1.2	,	
—- 231 -			
		•	•
232	1P40 * I + 44		
233	30 CONTINUE	• •	,
234	00 40 [= 1.2	•	
235 -	READ (5.190)-DJ(I)(XNB(I.J). J = 1.2)		• •
236	IP40 = I + 46		
237	40 CONTINUE		p on the Primer trans to Primer special special control on the
238	C		
239	C OUTPUT INPUT DATA.	•	A TO THE P & T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
240	J = 1		
241	00 75 I = 1,6		• • • • • • • • • • • • • • • • • • • •
242	JX = J + 4		
243			a man districted a acceptable acceptable
244	92 FORMAT(* 1.12.2X.5(F9.4))		
 - 245	ئىد 5 بان بىسىسسىد	N N N N N N N N N N N N N N N N N N N	پار بند او بوروسومیون وو و سخت جند ۱ دستو پرستس ا
246	75 CONTINUE		•
247			
248	J = 45		•
249	#RITE(6,92) J,RMT(1),RMT(2),DJ(1),DJ(2)		
. 250	C		• •
251	- C IF TTY I/O MAX.TIME WILL COME FROM WORK CARD	De manufacture of the ship of the C. S. seem g. s.	
252	IF(ITTY .NE. 0) C(15) = 9999999999		•
253	AT LATE OF GLASSIAN TO THE STATE OF THE STAT		
254	C FI(CO2)	•	
255		pagin di gamagan daga maka ka di di dagan da ayan yan	
	C FI(02)		
256			
- 257	T DUM2=C(32) T TT		
258	· C FI(N2)		
259-			
260	WORK = 0 .		
201	NORK2=0.		E-3
262	C METABOLIC RATE OF 02 CONSUMPTION IN TISSUE.		
263	RMTB*C1N(3)+C(26)	- " ''' - ''	
, 264	RMTB2=CIN(3)=C(26)		ිත Ω'
265			POR POR
266	TIHEOF=O.		
267	··· \DS=0.		
268	KMH=10.*C(36)/0.0078125		and the
269	т ~ нин≖о	·· · · · ·	
270	201 CONTINUE		(2)
271-			- · · · · · · · · · · · · · · · · · · ·
272	IF(MMM.EQ.1)XDS#XDS+C(36)		Principal Control
273 -		*** ** * *	
274	C(35)=0.		
275	C(40)=0.	•	
276	c		
278	C ARTERIAL CONCENTRATION OF CO2.		
· · - 279 -	CC(1) * Q+6 · ·	**** * * * * * * * * * * * * * * * * *	** ***** * ****** * *******************
. 280	C BRAIN CONCENTRATION OF COZ.		•
281	CC(2) = C(4)	•	A Company of the same of the s
282	C TISSUE CONCENTRATION OF CO2.		. w
283			2 200 200 - 200 200 - 200 200 - 200 200
284	C BRAIN COZ TENSION.		·
	C DIMIN COL ICHISTONE	•	
•	•		· • —

	/		
285	CPB = 50.0		,
287			
288·		•	
239	C SETS VARIOUS CONSTANTS AND AGGREGATES OF CONSTANTS		
	C- THAX.		
291	C(15) = C(15) + +0001		
 292			
293	c = c(39) = c(39) + *0001		
29 4 ·	C FACTOR OF 1-6-7 HULTIPLYING DIFFUSION COEFFICIENTS.		
295	00 200 [# 27.29		•
296	C(1) = C(1) = 1.E-7	-	
297	200 CONTINUE		
298	== :: =: :: * : * : *		
299	IRK = 1		•
300	· · · · · · · · · · · · · · · · · · ·	P * ***** ** * * * * * * * * * * * * *	
301	N * 5		•
302	IDd(1) m D	** ** 1	V ■
303	C SOLUBILITY COEFFICIENTS.		
	CA(1)*-(ALPHA)CO2+-A(2)=-(ALPHA)O2, A(3)= (ALPHA)N2+		
305	C A(4) = {ALPHA1CO2, A(5) = {ALPHA}O2, A(6) = {ALPHA}N2		•
306		••	
307	** A(2) = 0.024		
- 308	A(3) = 0.013	•	
309	A(4) = 0.51		•
310·	· · A(5) = 0.024 · · · · · · · · · · · · · · · · ·		
311	A(6) = .0.013		
312-	C- ATM/HHHG CONVERSION FACTOR.	•	to the second state of the
313	SK = 0.00132		
314	- C- CARBONIC ACID DISSOCIATION CONSTANT.	•	
315	CADK # 795,0	• •	
		LE- TIME-DELAYS+	
317	Vol(1) = 0.015		
318	· +0L(2) # 1.002		
319	VOL(3) = 0.188		
320	· · · · · · · · · · · · · · · · · · ·	4)
321	VOL(5) m D•188		
_			
323	VOL(7) = 0.735		
324	VOL(a) = 1.062	•	
325	AOF(4) = 0.998		
326	· VOE(10) = 1.002	• •	
327	C		
	C (METABOLIC RATE OF CO2 IN BRAIN + TISSUE.) / SAME FOR	02	
329	QF(6) = (C(25) + RMT(1))/(C(26) + RMT(2))		
330-	····································	•	
331	U(1)=C(30)+47.		•
	· 00 210 1 = 2,4		mm , or make the term of the second commence of the
333	C PRODUCTS OF CONVERSION FACTORS AND SOLUBILITY COEFFIC	IENTS.	•
334-	D(1) # 5K+A(1+1)		
335	D(1+9) * SK+A(1+2)		
. 336	c	• •	h #14## + #14### pag #4 # #### + ###### + #######
337	$D(1+3) = D(1) \cdot D(1)$		
338	· 210 CONTINUE		
339	C FACTOR USED IN ESTABLISHING CA(CO2)		٠ <u>س</u> ٠
340	D(8) # 0.16-4-2.3.C(17)		., <u>., ., ., ., ., ., ., ., ., ., ., ., ., .</u>
341	C .		

```
n(9) = 863 \cdot n/n(1)
 --- 343.
         -- C--FACTOR USED IN ESTABLISHING CB(CO2).
   344
                 D(10) = 0.62
   345
         --- C - MANIPULATION OF COMPUTER TIME STEP.
   346
                 D(14) = C(36)+2+0
              - - D(15) = D(14) - + D(16)
   347
   348
            C
   349
                 CALL Re3
   350
                 CALL RC4
- - - 351-
                 CALL RC5 (CP8, F(4), C(4), BC(2))
                 CALL RC21 (CHB(2), F(3), F(4), C(4), CH(2), CPH(2))
   352
                 CALL RC19 (CPB, CH8(2), CC(2), BC(1), F(4))
   353
                 CALL RCS (CPT, F(6), C(7), BC(3))
   354
   355
                 -CALL RC21-(CHB(3)+ F(6)+ F(6)+ C(7)+ CH(3)+ CPH(3))
                  CALL RC19. (CPT, CH#(3), CC(3), BC(1), F(6))
   357
                 CALL RC20
   358
                 CALL RC7
   359
                 CALL RCB .--
   360
                 CALL RC9
               -----CALL-RC10 ...
   3.2
                 CALL RC11
   363
            --- CALL RC12 ----
   364
                 60 TO 60
           - * - 58 CALL RC15
   366
                 CALL RC16
   367
               OD CALL RC13
   368
                 CALL RC12
   349
   370
   371
                  IF (C(35) .GT. C(15)) GOTO80
   372
   373
               -- IF(CXT.GT.C(15))-GOTC 80
   374
               70 CALL RC14
   375
          --- ' '-- UU # AMOD(C(35); D(14)) .
                  IF (UU .LT. .0001 .OR. UU .GT. 0(15)) G07050
   376
               -- RETURN ...
   377 -
                  GO TO 60
   378
            C
            ---- 80 WRITE16.78) "-- ..
.-- -- 379
               78 FORHATI'I FINAL VALUES FOR FOLLOWING VARIABLES. 1)
   380
               . IF (C(37) +GT+ 1+0E=5)
                                        GO TO 250
   156
   352
              220 CTERM # 0.0
                                            230, 240, 240 - -
----·3A3-
                  1F (YTRAN(14) - 104.0)
              23G CTERM = (23.6E-9) + ((104.0 - VTRAN(14)) ++4.9)
   384
             .240-C(37) = C(20)=(C(16)=yTRAN(15) + (1.0 - C(16))=CH(4))
                       + C(21) * VTRAN(13) + CTERN * VI
   386
   387
                 ARITE(6.192)I.C(I). (XN(I.J). J = 1.2)
   388
       · - - - 250 00 260 1 # 1+14.
                  ARITE(6.192)I.C(I), (xN(I.J), J = 1.2)
   390
             -260 CONTINUE ------
   391
   392
                 WRITE (6.194)
 -- 393
                  ARITE(6.830) -
             #3D FORMATIONORMAL TERMATION *)
 - 395
            301 CONTINUE
   396
                 STOP
       C 92 FORMAT (42XI3,10AF10+4,10X2A6)
```

	•	
Annual Company Company Company Company		
399 C'190 FORMAT (5XF15.0,5AZA6)400		
401 194 FORMAT (1H1)		•
452 · END		
★		
and which a construction from the first on the construction and the cons	•	per use order only a see section of the section of
-OPRT-5-RC+2	,	
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6-G03432+TPF5+RC12	•
SUBROUTINE RC12.	()) **** ***
2 COMMON/RINTR/ROUT(10),CIN(10)	
DIMENSION C(40), XN(40.2), SV(18.50), VTRAN(18), 1	RK(14,4),
4 T 1 Sc(14.5), Dc(14), A(0), D(15), F(20), V(DL(10), RMT(2),
5 2 BC(4), QF(6), TAU(5), CC(3), CHB(3), CH	(4), CpH(3),
6 3 DG(4)	
7	VOL. RMT BC. QF
8 1 TAU, CC. CHB. CH. CPH. DQ. VE. VI. CPB. CP	T, CADK, X, DT,
- 9 - 2 1RK, ĹOC, ITEKY, INDEX, 1, J. M. N	
10 COMMON/R/ XDS.XMH.CXT.AORK.DUM1.DUM2.DUM3.WORK2.RI	TTB,RMTB2,TIMEOF
- 11 - 1 .RMLIN.ITTY.ITTYOT.ITTYIN.WRKTTY(50.3).LEXEC.MA	RKER NWREST
12 2 RMTM.TCT	
- 13	
14 DATA IBACK/ BACK !/	
- 15 C - DIMENSION ARKTTY (50,3)	
16 C6969 FORMAT(1H BHSUB RC12)	
- 17 C - GUTPUT PUNCHED CARDS AND PRINTED	
18	
19 1F (CXT+LE+D+)CXT++O+	
20 C DEAD SPACE VOLUME	
21.4 95VOL#0.140+0.002.VE	
22 C RESPIRATORY FREQUENCY.	
-23 FREW=((1.+(.726+VE)/DSVOL)++.5+1.)/.363	
24 C DEAD SPACE VENTILATION	
- 25 DEAUVI=1.+.098-VE	
26 C (31)=(DEADVT+C(1)+VE+DUM1)/(DEADVT+VE)	
- 27 C C(32) = (DEADVT + C(2) + VE + DUM2) / (DEADVT + VE)	
28 C C(33)=(DEADVT+C(3)+VE.DUM3)/(DEADVT+VE)	
30 TYNT*DEAUVT+(VE+VI)/2.	•
31 C-HEART RATE	
- · · · · · · · · · · · · · · · · · · ·	
32	
34 C	
35 IF(CXT +LT+ TIMEOF) GO TO 203	
36 C	
-37	
38 C ' BRANCH IF IN BATCH MODE.	
39 1F(ITTY -EG+ 0) GO TO 500	
40 C	
-41 [*]	
42 C HERE IF TTY HODE	
-43	
44 C HERE IF TTY MODE. AND 1ST TIME THIS ROUTINE CALLED.	
-45	
46 mRITE(6,505)	
47 SQS FORMAL(*OINPUT WORK CARDS*/)	•
48 C 1 * WURKE HOKK LUADINATTS) ****/	
49	
SO C 3 * PRINT* TIME INCRIMENT(MINS)FOR PRINTOUT*/	
51 * EXEC+++*/	
52 C 5 * MORE INPUT MORE BEFORE EXEC 1/	
-53 -C - 6 ⋅ RIN = EXEC+HITH ABOVE.THEN CAN INPUT AGAIN++	
54 C 7 * STOP≈ EXEC+NITH ABOVE THEN STOP+++*/	
-55 8 * BACK* ENASE PREVIOUS HORK RECURD*)	
56 504 ITTYIN # 0	

- 1 1

```
ITTYOT # 1
 5.7
          501 IF(ITTYIN +LT+ 50) GO TO 506
-60 --- - -C HERE IF BUFFER FOR WORK I GAD CARDS IS FULL.
 61
             GRITE(6,511)
       - 511 FORMATI' GBUFFFR FOR WORK LOAD RECORDS FULL. 1/
            1 * WILL USE EXEC# RUN. 1
           · · LEXEC # IRUN .....
 65
             GO TO 551
 67
          506 ITTYIN = 1777IN + 1
    -- -- 509 WRITE(6.507)
 69
          507 FORMAT( ) NORK MINS PRINT EXEC 1.
          --- 1 1(F6.2,1X,F6.2,1X,F6.2,1X,A4)...')
 71
             READ(5.502.ERR#509) (WRKTTY(ITTY(N.J).J#1.3).LEXEC
-72
        - 502 FORMAT (FA.2.1X, F6.2.1X, F6.2.1X, A4)
             ARITE(6,503) (ARKTTYLITTYIR, J), J=1.3), LEXEC
 74 --- -- 503 FORMAT(3(1 1)F6-21,A41
             IFILEXEC +NE+ IBACK) GO TO 518
          ----ITTYIN- = ITTYIN = I
 77
             IF(ITTYIN +LT+ 1) ITTYIN = 1
--78----- GO TO 509 --
 79
       c
IF (LEXEC .EQ. MORE) Go To 501
      510 FORMATI' EXEC.PARAMETER WRONG. TRY AGAIN. 1
             GO TO 507
 86 - - C HERE IF IST TIME THIS ROUTINE CALLED.
        C SEE IF MORE WORK CARDS IN BUFFER(WRKTTY(500,3))
    C HERE IF EXAUSTED WORK CARD BUFFER ("RKTTY (500,31).
 90 -- - -- - IF (LEXEC .EQ. 18UN) GO TO 504
 91
        C FORCE END OF COMPUTER RUN WHEN LEXEC "STOP".
      - --- - C(15) = D. -
 93
             GO TO 1210
          551 WORK2 = WRKTTY(ITTYOT.1)
       --- DURAT # WEKTTY(ITTYOT.2)
             C(39) = ARKTTY(ITTYOT.3)
     GO TO 606
100
101
102
103
          203 IF (MARKER . EQ. D) GOTOINI
104 _ _
       1. WORK#JORK2
105
            . MARKER=1
    107
             IF (NGRK.LE.D.)GOTO2
108
             IF (HORK.GE.SO.) TCT=2.3/(2.**AORK/200.)
109
             IF ( NURK . LT . SU) TCT=4 . 6
110
        C TISSUE 02 HETABOLIC RATE.
111
             KMT(2)=SSU2N(NORK)~(SSU2N(NOKK)~RMTd2)*EXP(-TCT*(CXT -TIMEON))
112...
            --- wtime=1.1-1.1-Exp(-TcT+(cxT-TIMEOL)/1.42)
        C TERM USED IN VI THAT IS A COMPONENT OF TRANSIENT RESPONSE RELATED
```

	·		ر أي بالمستقدمين بالمستحد بلغاء ا
114	C TO WORK LOAD.		- c
115			· · · · · · · · · · · · · · · · · · ·
116	IF(VTIME.GE.1.) RNLIH=SSOZW(#ORK)	•	· · · · · · · · · · · · · · · · · · ·
117	C .TISSUE CO2 HETABOLIC RATE.		
118	MRMT(1)#.88+RMT(Z)	•	•
119	1F(TVNT.GT.37.) RKT(1)=(TVNT+40.77)+RMT(2)/88.5		
120	1F(C(35),LT,C(40)) G0T02		
121-			
122	333 FORMATE TOTALX, 25HCHANGE IN METABOLIC RATES, 5X, 7HMRCO	2= ,F10.4,	•
123	1 54.6HRR02= .F10.4,/)	a and the second of	
124	Ç		
. 125	c		
126	2 CONTINUE	•	
127-	IF (#ORK+LE.D.D -AND- NWREST+LT-1) RMT(2)=CIN(3)-C(26)		
128	$AVO2DH=(F(9)+C(10)-F(\tilde{1}3)+(C(10)-C(11))-F(12)+C(11))+100$	00.	
129	AVO2UF=AVO2DM/C(10) -	†	·
130	ROUT(1)=AVQ2UM/1070.		
131	ROUT(2)=FKED IF(WORK.GT.O.O) ROUT(1)=RMT(2)+C(26)	and nothing particles of the control	the transfer of the management of the management of the management of the same
132	ROUT(3)=C(11)	,	-
133			
134	ROUT(5)=F(1)		•
	C- " U = AMOD(C(35): 0:5)		
. 136	C 1F (U .LT. 1.DE-5 .OR. U .GT4999) GO TO 1210		•
137			
138	C(40)*C(40)*C(39)	1	'n
139	ARTERIAL NZ TERSION		
140	1210 PAN2 = D(1) • C(3)		
141	C. TISSUE 02 TENSION.		,
142	PT02 = C(8)/0(3)		
143	C TISSUE NO TENSION.		
144	PIN2 = C(9)/0(4)		
145	C CERESROSPINAL FLUID PH . EQUATION 6.2	*	
1'46	PHCSF = 9 RCF1(CH(4))		
- 147	C VENOUS BRAIN H+ CONCENTRATION . EQUATION 4.7		
148	HVB # CADK*F(4)/(CC(2) - F(4))	1	
149			
150	PHV8 = 9 RCF1(HVB)		•
151-			
152	HVT = CAD(-F(A)/(CC(3) - F(A))		
154	C VENOUS TISSUE PH , EQUATION 5.6 . PH/T = 9. ~ FCF1(HVT)		/ h
155	C - RESPIRATORY QUOTIENT (ALVEOLAR).		
156	RQ = ((C(11)*VTRA6.(4) + GF(1)*VTRAN(7))/C(10) = CC(1))/		
157-			· · · · · · · · · · · · · · · · · · ·
158	GF(5) = OF(6) = Rw		
159	· C	,	
100	č		
161	- C. HERE WHEN READY TO PRINT.		N 418 Part 1 18 Part 2 18
102	C SEE IF TTY MODE.		•
163.	IF(ITTY .Eq0) GO TO 610		
164	c		, "
165	C HERE IF TTY OUTPUT.	•	**** 1
166	HRITE (6.700) CXf,CC(1).CC(2),CC(3),F(9),F(12),F(13).		•
- 167	6 CH(4),F(7),CP8,CPT,F(1),F(17),PT02,VI,VE,C(11),		a mera p 1 m m _ m
148	6 FREQ.TVNT.AVOZDF, RMT(2), C(10)		40
- 169	- 700 FORMAT(7F9.4)		
170	RETURN		
<u>.</u>			
•	ı		
-			

,

```
171
               610 IF (R .NE. 4)
                                      GU TO 1270
   172
                   N # 0
   173.
                   naite (6.1805)
..... 174
            - 1220 N # # + 1
   175
             C
---- 176
                  -HRITE (A.1810) CXT: RO. OF(5)
   177
             c
                --- WRITE (6,1815) = (C(1), L = 1,3), (DC(1), L = 1,3), F(7), F(1).
   17A
   179
                         PAN2
                                     CC(1), F(9), F(10), F(/), F(1), PANZ, CH(1),
                   481TE (6.1820)
   180
                          CPH(1) . CH8(1)
   181
                                     (C(1), 1 = 4,6), (OC(1), 1 = 4.6), CPd, F(17),
                   WRITE (6.1825)
   162
                          F(18), CH(2), CPH(2)
   183
                                     (C(1), 1 x 7,9), (pc(1), 1 x 7,9), CPT, PTO2,
  - 144
                 - 4817E '(a.1830)
                         PTN2, CH(3), CPH(3)
   135
                                     (OC(1), 1 = 12,14), (C(1), 1 = 12,14), CH(4),
                 - WRITE (6.1835)
   106
   167
                         PHCSF
                                     CC(Z). F(12), C(6), CPs, F(17), F(14), HVB+
   188
                   (CARITE (6,1840)
   189
                          PHVB. CH8(2)
               --- WRITE- (6,1845)
                                     CC(3), F(13), C(9), CPT, PTU2, PTH2, BVT. ... -
   190
   191
                          PHVT, CH2(3)
                  WRITE (0.1850) (TAU(I), I = 1.5), VI, VE, C(10), C(11), DC(10). -
  - 192
   193
                         00(111)
                   WRITE (6,1855) FREG. TVNT. DEADVT. HRATE. AVOZDF. DSVOL
   194
   195
              1230 RETURN
--- 196
          - - 1290 FORMAT (5H XXXX5X7F10.4)
              1292 FORHAT (8F10+4)
   197
---- 198
             1805 FORMAT (1H1)
              1810 FORMAT (IMDOXYHTIMEFID.4.74KOYALV RWFIC.4.3X7HRQ DIFF.F8.4/
   177
                         16x3hcu28x2h028x2hJ27x21HD E R I V A T I V E SYX4HPCQ26X
  _ 200
                  - 1
   201
                          3HPQ27X3HPN27X4H(H+)7X2HPH5X4HH802)
 -- 202 --- -- 1815 FORMAT (3X8HAL/EGLAR9F10.4)
              1820 FORMAT (3A8HARTERIAL3FID.4.30X;5F10.4.F8.4)
   203
             1825 FORMAT (6X5HBRAIN) IFIn.4) .
._ _ 204 _ __
              1830 FORMAT (5A6HTISSUELLF10.4)
   255
   256 .
              1835 FORMAT (8X3HCSF3QX8F1C+4)
              1840 FORMAT (4A7HV BRAINSFIG.4.30X.5F1G.4.F8.4)
   207
             1845 FORMAT (3x84V TISSUE3:10.4.30x,5F10.4.F8.4)
 _ 208---
              1850 FORMAT (5418HTRALSPORT TIMES --487HAbeA2HVB8X2HVTBA2HAT8XZHAC24
   209
            1 2H * * 4 X 2 H V 1 & X 2 H V E 8 & 1 H O 9 X 2 H F & 7 & 1 1 H D E R I V A T I V E 5 / 2 I & . 1 O F I O . 4 . F & . 4 }
   210
              1855 FORMATISX. SHRESP FRE, G. F. 6. 4. 2% . I SHILL NOTE VOLUME . FB . 4.
   211
                  1 24.8HD S VENTAFBARAZXALBHPEAKT RATEAF844.
   212
                  2 2X.7HAVO2DF.F8.4.2X.5HUSVGL.F6.4)
   213
                 BATCH MODE WORK CARD KEAD ...
  . 214-
   215
                   WILL USE WORK CARD WITH TIME " G AS INDICATION
             C
   216
                   OF END OF RUN BECAUSE 1106 HAS PROBLEM
   217
             C
           ___C . TITH END# On READ.
   218
              SOO READ(5,,300,E,D=2) WORK2,DURAT
   219
           . 300 FORMAT(F6.2.31.F6.2)
   _22Q_
   221
                   IF (DURAT .GT. D.) GU TO 606
   222
             C HERE IF READ INDICATION OF END UF RUN IN BATCH MODE.
   223
           .. . . C(15) = D.
   224
                   GO TO 1210
   225
  __ 224
                ______
               ADA WRITE (A.305) AURKZ, DURAT, CXT
   227
```

			6 n n n n n n n n n n n n n n n n n n n
228	305 FORMAT(101,43(1+1)/		
229	1 * HORK LOAD CHG+(*+FA+2, **ATTS FOR ! +		
230	2 FB.2. *MINS) AT* , F9.4. *MINS*)		
231	607 TIMEDF=DURAT+CXT		*
232	T! MEON#CXT		
. 233	C. SYSTEM RESPONSES! TIME CONSTANTS FOR WORK LOAD	S AND TISSUE 02	
234	C METABOLIC RATE.		
235 -			
236	C DECREASING NORK LOADS.		
237		es y a mean v	ها منظری الحدود به الحدود ا
238	IF(HORKZ-LT, HORK) KNTB=\$\$02+(HORKZ)	ED 2//2 AND DE /200-1	•
239 240	1F((10RK2+LT+XORK)+AND+(10RK+GE+5C+))	~ 2.37 (2.4 WURN) 2004)	• •
241		•	
242			
- 243	- MARKER#O		
244	1.2 R 6 S T = 2		· ·
245	TO TISSUE 02 METABOLIC RATE.		
246	RMT(2)=RMTB=(RMTB=RMTM)=EXP(=TCT*(CXT=TIMEO	N) • • 50)	•
247 ·	YTIME#1.1-1.10EXP(-TCT+(CXT-TINEON)/3.84)	parameter as as an energy or energy and a second	
248	C TERM USED IN VI THAT IS A COMPONENT OF TRANSIE	NT RESPONSE RELATED	
2 - 9	C TO WORK LOAD+		
. 250	RULLY =RHT8=(RHT8=RMTM)=(1.~VTIME)	•	
251.	TECVITAE+GE.1.) MML1 V=MHTS		
252	C TISSUE COZ METABOLIC RATE.		
	R47(1)*.88*RHT(2)		
254	1F(TVXT.GT.37.) RMT(1)=(TVXT+40.77)*RMT(2)/	88.5	
255	IF(C(35).LT.C(40)) GOTO2	No. 4 No. 40	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
256	#RITE (6.333) RHT(1) .RHT(2)		J
- 257	G070Z ·	• • • •	
258	END		
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GPRT.S	\$502%		_
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086-G03432*TPF\$.5502m		
	an and a second a second of	, , , , , , , , , , , , , , , , , , , ,
2 C CALCULATION OF STEADY-STATE DAYGEN REQUIREMENTS F	OR VARIOUS LEVELS	•
3 C OF HORK LOAD (X#HATTS).		
4 4 COMMON/RINTR/ROUT(10).CIN(19)		
6 \Q2\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		•
7 KETURN	,	
8 END		
a. d galaxi levery		
SPRT.S TERG	,	
	- •	, , , , , , , , , , , , , , , , , , , ,
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DRAWGDS	432 TPFS+	FRG		
		- SUBROUTINE TERG		·
2	C***	GE CARDIOVASCULAR LENP MODEL 10/23/73	,	
3		COMMON/STATE/X(50).XDoT(50)		
4		Z/STATE/LRA,ORV,QLA,ULV,QPA,OPC,QPV,QAA,WARC,QLAA,		
5		34LABA-OCILL. WEGSA-GEGAR, GEGCAP. CEGVE. GEGSV, GFEY. W	ABVC, QTHVC, QSPVC,	t many transaction of the
6		HULOC, DUPC, OHCAP, OHSV, DUV. DCOR, CCSMA, CINA, GCSMV, QP		•
 7		SWPENA. GRALE, PREMY, WRET, OD(10), WSKB	- +	
8		6/STATE/CRA.CRV.CLA.CLV.CPA.CPC.CPV.CAA.CARC.CLAA.	CUTA, CL FA, CUABA,	
9		7CLAHA, CCILL, CLUSA, CLUAR, CLUVE, CLUSV, CFEV, CABVC, CT	HVC+CSPVC+ = = =====	· · · · · · · · · · · · · · · · · · ·
10		BCLOC, CUPC, CHSV, CJV, CCRMV, CIMV, CPOV,		
1 1		9CRE IA . CWEYV . CO (10)		A T Mar I warm I make as
12		A/STATE/PRA.PRV,FLA.PLV.PPA.PPC.PPV.PAA.PARC.PLAA.	PUTA,PLTA,PUABA,	
13		BPLABA, PCILL, FLGSA, PLGAR, PLGVE, PLGSV, PFEV, PABVC, PT	HVC.P5PVC	
1 4		CPLOC, PUPC, PHSV, PUV, PCSMV, PINV, PPOV,		
15		DPRENA, PRENV, POLICIO, PRO, PMC	-• • •	* *
16		COMMONISTATE!		·
17	-	ERPA. KHY, RMY, RAY, RPA, RPC, PPV, RARC, RLAA, RUTA, RLTA, RI		
18		FREADA. RCILE, REGSA. REGGAR, REGCAP, REGVE, REGSV, RFEV, R		•
19	···	GRTHVC.RSPVC.KLOC.RUPC.RHCAP,RHSV.RJV.RCOR.RCSMA.R	IHA i RCSMV ,	
20		HdPov, Rimv, PRENA, drale, BREFF, drenv, Ro(11), RSK8		
21	-	i/STATE/FLPA,FLAA,FLAKÇ,FLLAA,FLUTA,FLLTA,FLUABA,	male en ar mana a	maa seesa aysa aega .
22		JFLLABA, FLCILL, FLCSMA, FLIMA, FLRENA, FLDM(8)		•
- 23		K/STATE/V(50), VU(50), PG(34), PEXT(32), E(4)	** * ***	A MI A MI A A A A A A A A A A A A A A A
24		.PRN.ABIAS.TBIAS.TTHAT.THODEL.SPACE(5)		
—- 25		L,Z(40), WK(27), HR,SV,CA,RT,PEX,W,PSYS,PDYS,FREQ		
26		M.+VO200T,AVJ.PIA.B.PITH.PMP.THETA.SF		_
27	-	N.TTOT.TAS,TYS,C1,C2,GNEW,PEXINATR	* 10 mg/m / 200 MM gap ng-m- p-	
28		.DUMMY(13).T.OPRT.VLEG		ਾ <u>ਡ</u>
29		CALL AID		
30		CALL CONTRL		Q Z
31		TALL CVS	<u> </u>	ORIGINAL OF POOR
32 33		CALL ALGO(T)		
34	,	IF (T.GT.TTHAZ) THETAEO.		QUA PAGE
-		IF (T.LT. AK(204) GO TO 1		5 2
- 35 36	7	CALL EXEC	· · · · · · · · · · · · · · · · · · ·	Francisco (1973)
·· - 37		- END	· · · · · · · · · · · · · · · · · · ·	
3,	•	CND	***************************************	3,0
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SPRT.S	ćvs	AND A CONTRACT OF THE A CONTRACT OF THE CONTRA	5	
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<u> </u>	·		20)	
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D86~GD3432*TPF\$*CVS	•	•
1 SUBROUTINE CVS		•
2 C GE CARDIUVASCULAR LBNP MODEL		* *************************************
3 - C CUNTROLLED SYSTEM		
4 COMMON/RINTR/RIN(10), POUT(10)		
	•	•
5 COMMON/STATE/X(50), XUAT(50)		
6 2/STATE/ORA, GRV, ULA, LLV, OPA, OPC, OPV, SAA, WAKE, GLAA, G		
- 3GLABA-GCILL-GLGSA-GLGAR-DLGCAP-GLGVE-GLGS/-UFEV-DI		
8 40L0C,040L0C,04CLP,07C,VCTC,VCTC,4CSA,6[AA,6]	on a mina	·
9 · SURENA GHALE . LRENY , OR E TO OD (101 , WSAR		out the service of our secondaries, service or
10 6/STATE/CRA.CRV.CLA.CLV.CPA.CPC.CPV.CAA.LARC.CLAA.C		
11 - 7CLADA-CCILL.CLGSA.CLGAR.CLGVE.CIGSV.CFFV.CABVC.CT	ivc,CSPVC.	* *************************************
12 8CLDC.CUPC.CH5/.CJV.CCSMV.CTMV,CPUV,	•	
13 9CRENA.CHENV.CD(18)		
14 A/STATE/PRA.PRV.PLA.PLV.PPA.PPC.PPV.PAA.PARC.PLAA.F	PUTA, PLTA, PUABA,	*
15 BPLABA.PCILL.PLUSA.PLGAR.PLGVE.PLUSV.PFEV,PASVC.PTF		
16 CPLOC, PUPC, PHSV, PUV, PCG'IV, PTMV, PPOV,		
17 DPRENA.PRENV.PD(16).PM.PMC		
18 COMMON/STATE/		
19 ERRA, HRV, KHV, RAV, RPA, RPC, RPV, KARC, HLAA, KUTA, RLTA, RL	P. 11. A	,
The state of the s		•
The dividio dividio de de la contrata del contrata de la contrata de la contrata del contrata de la contrata del la contrata del la contrata de la contrata del la contrata del la contrata de la contrata de la contrata de la contrata de la contrata del la contrata	MA, KCSMV, -	
HRPOV.RIMV.RREHA. HRALL. RREFF, KREHV, HO(111, R5K8		
23 1/STATE/FLPA.FLAA.FLARC.FLLAA.FLUTA.FLLTA.FLUABA.	• • •	
Z4 JFLLABA, FLCILL, FLCSMA, FLIMA, FLRENA, FLUM(3)		
25 K/STATE/V(50), YU(50), PG(34), PEXT(32), E(4)		
26 • PRR, ARIAS, TBIAS, TTHAT, TMODEL, SPACE (5)		
27 L.Z(40), %K(20), HR, SV, Co. RT, PEX, H, PSYS, PUYS, FREQ	- /	,
28 M.VO2DOT.AVD.P1IH.PMP.THETA.SF		
29 N.TTUT.TAS.TVS.C1.C2,GMEW.PEXIN.TH		ي موسيد او المستند و دار المساور در المساور و الماد ال
30 •.OUNY(13),T.OPRT,VLEG		•
31 DIMENSION PRS(1), CMP(32), R50(50), FINR(12)	<u> </u>	
32 EQUIVALENCE (PRS, PRA) . (C4P(1) . CRA) , (RSO(1) . RRA) , (F	INR(1).FLPA)	
33 6 (PD(3), IT), (PD(4), TG/E), (PD(5), TRSP), (PD(6), TMP)		
34 & .(PD(\), TPS),(PD(a).P2)		•
35 - C - T IS ELAPSED TIME		
36 C TT IS A CLOCK FOR ONE BEAT)
37 TT=T+TSVE		
21 - 11=1-1245	• •	A. C
39 - 1001-TSVE=T	•	•
40 C		,
- '~ 41 DP4D#1700+44600+/3++(V02D0T-+6) -		At the state of th
42 (064-7940-80) · ·		
- 43 iF(DPER-LT50-)PO()11;=PO()11001	وي بيد وه و يا مستوي و حد و	
44 IF(DPER.GT.50.)PO(11)=Pn(11)+.001		•
45 · IF(VO2DOT-LT5)PD(11)=Q.		
46 C0=X(33)/TTOT06		•
47 x(33)=0.0		<u> </u>
48 Pn×4(10)/TTO(
49 X(10)=0.0		•
50 PHC=X(13)/TTOT		
51 X(13)=0.0		
52 PO(1)=4(34)/TTOT		
53 - X(34)=0.0		
The state of the s	•	45
		Ct
56 DIFF==V(50)+V(4Y)	•	

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•	•				-	
57	X(18)=X(13)+D1FF+0+6					•
58 -	X(19)*X(19)+U1FF+0+4 -					
59	PSYS≖SYS .					
60						
61	CALL XIO					
62	PO(10)ac.					• • •
63	110 CALL CONTRL					
———— <u>64</u>	TEMP+0.2	, , , , , , , , , , , , , , , , , , , ,				
45	IF (TEMP=T) 110,111,111					
46	· 111 CONTINUE		•		**	
67	CALL EXEC			,		
48	· 5Y5#40			,		
69	072=1000+					
70	TTOT=60./HR -	-	· · · · · · · · · · · · · · · · · · ·			
71	TAS=0+10+0+09=TTOT					
72	TVS=J+16+0+20=TTOT		1	•	•	
73	IF (T.LT.41. OR. T.GT.	43.1 GO TO 20				
74	00 10 1=1.32 '		•		· —	
75	10 PG(1)=SIN(THETA/57.2958) +Z(1) +1.05 + y 80 • \ 1332	•			
76	TILT=THETA				······································	
77	20 CONTINUE	•			•	
78	IF (TMODEL.GT.D.) GO TO	59				
79	GO TO 30					•
80	- C- 26 IF (ABS(THETA)+LT+1+E-5		30			
61	26 IF (AUSTTHETA) - GT - 1 - E - 5					
82	IF (ABS(THETA).GT.1.E.S		· · · · · · · · · · · · · · · · · · ·		~ ~	******
83	IF (TILTD-GT-2-1 GO TO :	30			ÖRÎGINAL OF POOR	
84	DD 20 [-1132	•	·		<u>-</u>	
85	28 PG(1)=0.			•	┌──	
.86	TILTD=3.	,			8 €	
67	30 CONTINUE				<i>≒</i>	
88	VEEG=0.	•••	· · · · · · · · · · · · · · · · · ·		<u> </u>	•
90	00 201 1=15.20				PAGE	
91	VLEG=VLEG+V(1)	,			56	
92						•
	VLEG=VLEG=VU(18)=VU(19).	- VU (20)				
93	TEMPV=0.				3 5	
95	. 16 TEMPV=TEMPV+VU(1)					
96-	SPACE(3)=V(50)-VLEG-TEM		·		•	
97	·	-4440116/14401177440121	.,			
- 98	6 +VU(15)+VU(14)+VU(17) 					
7.9	[F(TT+TAS)1,2,2	*			***	
100-						
101	£(1)=0.05+0.05+5AS+SF	-				
102	E(3)=0.12+0.14+5AS+5F					
103	RSPVC=(20++5A5++0+)/1332	.	·- · ·	•		,
104	RTHVC=(10++SAS+20+1/1332					
105	60 10 3	· -			•	,
	2 E(1)=0.05		$\epsilon = -$			
137	E(3)=0.12	•		• • • • • • • • • • • • • • • • • • • •		
100	RSPVC=-015015			*		
109	KTHVC=.0075075					
. 110	3 TV=TT=0.1	•	•		•	•
111	IF(TV.LT.0.0)TV=0.0					4
- 112-	if(TV=TVS/4,5,5					. 0.
113	4 SVS=5[N(3.1416=TV/TVS)				, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
-,	4 242-214(241410-14)(42)					
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114	£(2)=0.01/5+.39*5F*5V5		
115	E(4)=0.02+1.50+5F+5V5		·
116	GO TO 6		•
·	E(2)=0.0175		, , , , , , , , , , , , , , , , , , ,
118 😽	E(4) =0.0Z		•
	CONTINUE	•	
120	00 11 [=1.4		
	Cmp(1)*1*/E(1)		
122	\$F(X(4).LT.0.0)X(4)=0.0		•
123 C -	COMPUTE VOLUMES	•	
124	V(50)=0.0		• • • • • • • • • • • • • • • • • • • •
- 125	00 55 [=1,32	_	
126	A(1) = A7(1) + X(1)	-	
	- V(501=4(53)+V(1)		
128	V(50)=V(50)=V(7)=V(11)=V(13)=V(10)=VU(18)=VU(17)=VU(20)	3	,
	1F (INETA . GT . 45 . AND . T. GT . 40.) PITH = -2.5		
139 C	RESPIRATORY PUMPS		
	· IF (PEX.EQ.3.0) 60 TO 115		•
132	1F(T-LE-40-0 +0K+ THETA-LT-45+)GO TO 115		, " ,
	trsp=trsp+t=TP5		
134			
	IF(TRSP.GT.TR)TRSP=3.n		•
135	71*Td5p/IR	 T:-eu	· · · · · · · · · · · · · · · · · · ·
136	PITH#~2.6/~19.704*T1+66.409*TI*#2~53.479*TI**3*16.602*T	14441	
137	JEPTH=(V0200T=1+)/2+		***************************************
138	IF(DEPTH.LT.O.) SEPTH#A.		
- 139	if (DEPTH.GT.1.5)DEPTH#1.5	,	
140	P1TH=P1TH=0EPTH	•	,
• ' •	PIABEMP1TH/2+		
	CONTINUE		
,143	00 71 1#1,12		
144 71	PEXT(I) #PITH		
	- PEXT(22)=P1Td	1	* * * * * * * * * * * * * * * * * * * *
146	PEXT(23) =P174		
147	00 72 1=26,32		
	PEXT(I)=PIAB		
149	SEXI(14) alive	1	
150	PEXT(21)=Plad	,	
151 - "C	MUSCLE PUMP . "	مستواها بمراب والمراب	· ————————————————————————————————————
152	IMP#TMP+T-TP5	* **	
7 153 "	TPS#T	~	ــــــــــــــــــــــــــــــــــــــ
154	IF (TMP.GE.1.) TMP=0.	,	
155	SMP#5111(Z++3+1416+TMP)	· · · · ·	ب ما در ما المراجع الم
156	PMP=40.esMP	,	
- 157	IF(THETA.LT.15.)PHP#10.*SMP		
158	IF (5MP.LT.O.) PMP=0.		
· ·- 159	1F (PEX.LT.1.) ₽M₽#0.		<u>ــــــــــــــــــــــــــــــــــــ</u>
160	DO 44 1=16.19		
161 - 44	PEXT(I) #PMP	•	· ·
162 C	COMPUTE PRESSURES		
	P1=P2		
164	P2=PLV		
1 65	00 12 [#1:7		
	PRS(1) = x(1) / CMP(1) + PExT(1)		
	OPDT#(PLV=P1)/(2.4.007)		The second of th
168	1F (OPOT - GT - PU(10)) PO(10) # OPOT		45
- 169	00 13 [#15,17	•	· · · · · · · · · · · · · · · · · · ·
170 13	PR5(1)=x(1)/CMP(I)+PExT(1)	•	•
	•		
		•	V - V - V

•			•		
171	PTIS=SPACE(4)				`
· 172 -	PGBIAS=SPACE(5) -			··· - ·-· <u>-</u>	· · · ·
173 •	00 15 (x18,20				
174		.+PEXT(I)+PTIS+PGBIAS-	2.		
175	15 1F(X(1).GT.VU(1))PR				7. A.
176		1)+PEXT(1)+PTIS+PGBIAS			
177		174FEX111741 11341 00143			
	DO 14 1=24,32				
178		PEXT(1)			
179	PAA=X(B)/CAA+PITh				
1 80	PUTA=X(29)/CUTA+HIT				to the same of the
151	PLTA=X(12)/CLTA+PIT	Н			•
182	IF (PUTA.GT.SYS)SYS#	PUTA	,		
183	IF(PUTA-LT-DYS)DYS#	PUŢA			
184 -	PLABA=PIAS=11.826+0	·0-2765+V(14)+0-009773	4-7(14)-7(14)	} <u> </u>	
185	PLABAMX (14)/CLABA+P	IAR			•
- 186	Cases ABDOMINAL VENA CAVA				
187	· · · · · · · · · · · · · · · · · · ·	40a*y(21)-0*00033598*V	(21) eV(21)		
- 188	-" .+0.000nn045p26+V(21				
189	IF (A(21) • GT • 200 • •	•			
- 190					·
-		217-70017-1113			
191	C. THORACIC VENA CAVA		0 t = 11 t 0 0 t		
192		4 • v (22) • 0 • 00065673 • v (2	2144(22)		
193	.+0.00Con1236.v(22).			•	
- 194	- ' IF (A(22) - GT - 150	- · · · · · · · · · · · · · · · · · · ·			
195	. PTHVC=.3/100. * (X	•			
196	P52VC#=3.4999+0.924	U9-1(23)-0.042246*X(23	} + X { 23 }		
197	,+8.00063485+x(23)+x	(231+x(23)			
198	THVC=PTHVC+PEXT(22	TTBIA5 " '	- •		
159	PAGVC=PARVC+PEKT(21)+481AS			
203	- PSPVC=PSPVC+PEXT(23	, -			
201	QRA=(PPA=PRV)/RRA			•	
202	HEART HUDE				
203	IF (PRA . L T.PR.) SKA=0	_			
204	- · QRV#X(09)/FLPA				
235	1F(QRV.LT.0.0) 4KV=0	. n			
	-				
~~ 206 ·	V0011071=LX1=LVHVX		\=D. 0		
207	4	AND + GRV + EQ + O + O) X D OT (0 9	7-0-0		•
208 '	" GLA=(PLA-PLV)/RHV	•			
209	IF (PLA . LT . PLV) OLA #0	• U			
210	" QLV=X(11)/FLAA	•			
211	. IF(QLV.LT.N.O)QLV±O			•	
212 .	XDOT(11)=PIVTPAA+PG		•	,	,
213		AND OLV . EU . D . D) X D D T (I I)=0.0		
214	— C ↑∪L⊣n'+\RY (CIRCULATION			*
215	/ / GPA=(PPA=PPC)/RPA				
519 .	QPC=(PPC-PPV)/RPC		••••		
217	OPV=(PPV=PLA)/KPV	•			•
21g	C ARTERIAL M	ûDFL			, , , , , , , , , , , , , , , , , , , ,
219	GAA=(PAA=PUTx+ru(12				•
- 220					
221	QLTA=(PLTA=PLABA+PG				
	QLABA#(PLASA=PC!LL+				
		LOCIPLIANCING		•	· · · · · · · · · · · · · · · · · · ·
223	C LEGS	n			•
224	QCILL*(PCILL+PG(16)				, , , , , , , , , , , , , , , , , , , ,
225	QLGSA#(PLGSA-PLGAR).	•			
226)/RLGCAP		•	
227	RLGVE≈.OS		•		

			•
	QLGVE-LT-J-0)RLGVL=67-56/56/ VE=(PLGVE=PLGSV)/RLGVE		٠,٨
	5V=+05		,
_	0LGSV.LT.0.01RLG5V=67.567567		, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,
• •	5V=(PLGSV=PG(19)=PFEV)/RLGSV		
—· 233	VENDUS MODEL	r	
	V#.021		•
	QFEV.LT.0.0) RFEV*67.567567		·
	V=(PFEY-PG(2D)-PABVC)/RFEV		•
QAB	VC=(PABVC=PG(21)=PTHYC)/KABVC		
238 QTH	VC=(PTHVC+PG(221-2RA)/RTHVC		
239· QSP	VC#.(PSPVC-Pu(23)-PRA)/RSPVC		
240 C	HEAU+ARMS	•	
_	C=(PAA+PG(24)=PLOC)/RLOC		
	C#{PLOC=PUPCI/RUPC	•	
· ·	AIN#RIN(3)+1000+/6n+	· ••	, not a manage of the franchise of
<u> </u>	M=17 = 25		
- · · · · · · · · · · · · · · · · · · ·	AP=OdRAIN+GARH CAP=(PUPC=PHSY)/RHCAP	• •	
	A=(bH2A-b1A)\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		,
	*•004301		
The state of the s	QJV.LT.0.31KJV#67.567567	•	• ***
	={PJV=PG{27}=PSPVC1/RJV		
251	CORUNARY CIRCULATION		
252 900	R=(PAA=PPA)/RCOR		
253 · C	CONTINUITY FOR VENOUS RETURN		
	T#QSPVC+@THVC+#COR	•	
255 - C ·	HEPATIC-SPLANCHNIC CIRCULATION	•	,
-	MARIPETA-POSHVI/RUSHA		•
	MV=(PCSHV-PPOV)/RCSHV V=(PPOV-PTHyc)/RPOV		
259 C	- RENAL CIRCULATION		m :
	NA=(PLASA=PRENA)/RRENA		
	LE=(PRENA-PRENY)/(RRALE+RREFF)		, , , , , , , , , , , , , , , , , , , ,
· 202 QRE	NV=(PRENY=PABVC)/KRENV		
- 263 - C - ,	SKELTON-DONE MARROW-AND OTHER	P 44	
264 QSK	a=(PLAnA-PAnvC)/RSK3	*	·
	STATE VARIABLE DERIVATIVES		
•	T(1)=JRET=QKA		•
	T(2)=GRA=GRY		/
·	T(3)=49PV-0LA T(4)=0LA-0LY		<i>(</i>
	((1)#90A-V[? ((5)#9RVPA		
	T(6)=3ピムーッドC		,
	1(7)=uPC-wPV		
= 273 · · - ×00	T(S)=uLV=uAA=@CGH=nLOC		
274 م	T(10)=PAA	•	
275 XOD	T(12)=GOTA=GLTA=GCSHA		end of an end of depolarization
	T(14)=_LTALNMA-WRENA-GSK8		
	T(15)=WLABA-GC:LL		
	T(16)=3CILL-WLGSA		
	T(17)=WLGSA-GLGCAP		,, ,, , , , , , , , , , , , , , , , ,
	T(18)=4LGCAP-4LGVE T(19)=4LGVF-4LGSV	•	
The state of the s	17(20)=1LG5V-1FEV		
	T{21}==FEV====0=C+==ENV+=SKB		\$
	T(22)=LABVC+UPOV=STHVC		·
,	· · · · · · · · · · · · · · · · · · ·		
;			
		}	

•			
zas	XD0T(23)=QJV-QSPVC	r	
286	x00T(24)#3L0C+wuPC	+	* ************************************
287	ADOT(25)=QUPC-QHCAP		
288	T XDOT(26)=@HCAP=QHSV	•	
289 .	XDOT(27)=2hSY~UJV		
290	ADOT(28) #4CSMA-QCSMV	•	T 10 10 10 10 10 10 10 10 10 10 10 10 10
291 292	ATOT (29) = JAA = GUTA		
293			- · · · · · · · · · · · · · · · · · · ·
294			
295	X00T(33)=4LV		
296		a 1.	
297	XDOT(34)#PUTA		
298	RETURN		
299	CNB		
	• •	مست بسبب یا د جب ز	and the second of the second o
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		** ************************************	· · · · · · · · · · · · · · · · · · ·
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D86-G03432-TPFS	CONTRL.	-
2	COMMUNISTATE/X(501,ADdT(50)	•
	2/STATE/WRA, ORV, WLM, OLV: OPA: OPC: OPV: OAA; WARC: OLAA: WUTA: WLTA: WUABA;	
4	BOLABA, TOTILL, ULGSA, TLGAR, TLGCAP, OLGVE, ULGSV, UFEV, UABVC, UTHVC, QSPVC.	•
	44LOC, JACADA, VHRDG, AND	****
<u> </u>	SURENA ORALE ORENA ORET DO (10) SEKA	
	6/STATE/CRA,CKV,CLA,CLV,CPA,CPC,CPV,CAA,CARC,CLAA,CUTA,CLTA,CUABA,	
, 8	7CLABA, CCILL, CLGSA, CLGAR, CLGVE, CLGSV, CFEV, CABVC, CTHVC, CSPVC,	
	SCLOC, CUPC, CHSV, CUV, CCSHV, CIMV, CPGV,	برين پير ۱۹۰۰ کا د اداليس پير د در در پير پيروا
10	PCRENA, CRE, V, CD(18)	
	A/STATE/PRA, PRV, PLA, PLV, PPA, PPC, PPV, PAA, PARC, PLAK, PUTA, PLTA, PUABA,	
12	BPLABA, PCILL, PLGSA, PLGAR, PLGVE, PLGSV, PFEV, PABVC, PTHVC, PSPVC.	
	- CPLOC, PUPC, PASV, PUV, PCSAV, PINV, PPOV,	
14	DPRENA, PRENV, PD(16), PM, PMC	
	- COMMON/STATE/	
	ERRAPRRY, 34V, RAV, RPA, RPC, RPV, RARC, RLAA, RUTA, RLTA, RUABA,	
16 .	T. T. August and Augus	,
• •	GRIHVC.RSPVC.RLOC. RUPC. RHCAP. HHSV. RUV. RCUR. RCSMA. RIMA. RCSMV.	
18	HRPOV, RIMV, RRUMA, RRALE, RREFF, RRENV, RD(11), RSKB	
20	1/STATE/FLPA.FLAA.FLARC.FLLAA.FLUTA.FLLTA.FLLAA.FLUABA.	
21	JELLABA, FLCILL, FLCSMA, FLTMA, FLRENA, FLDM(8)	
	K/STATE//150), VU(50), PG(34), BEXT(32), E(4)	
22		
23	+ PRN, ABIAS, TOTAS, TTHAY, THOUGH, SPACE (5)	
. 24	L.Z(40).uk(20).mk.Sv.Co.RT.PEX.W.PSYS.PDYS.FREQ M.VO2DOT.AVD.P1Ad.P1Th.P4P.THETA.SF	
26	NITTOTITAS, TVS.CIICZ, GNEA, PEXINITE	· · · · · · · · · · · · · · · · · · ·
27	- •, DUMNY(13), T. DPRT. VLEG	
28 CC	CVS-RESP. INTERFACE BLOCK DATA FOR INTERFACE IN & OUT	
29 C - 30	COMMUNICALINATERIALE IN & OUT	,
~~	<u> </u>	
· ·	INPUT FROM RESP.	
32	V0200T=RIN(1)	
7 33	- FREWHRIN(2)	•
34 C	33RAIN=RIN(3) •1000 • /6n •	
35	PC02=R[N(4)	
36	P02#R1H(5)	
37 ·	DPC02=PC02=37.5751 "DP02=P02-107.9482"	
		*
39	RVACT=1.=(10PC02+0P02)+0.01273] RVACT=1.	
.40 C	- OUTPUT TO RESP.	*
42	ROUT(i)=Co	
· -	ROUT(2) = V02D0T.	
44	ROUT(3) = RESTO2	
, •	•	
• 45 C 46	REAL NUMBO	
	- AQUIVALENCE	
	2 (ACCHET, K(41)), (XN4, K(43)), (DK, K(44)), (DL, X(45)),	,
46	- 3(DO2.X(48)).(X:3.X(49)).(PD(2),FLAG).(PU(9).UTS).(PD(12).DMS)	·
•	COMMON/DELAYO/ AVUTS(50).VOZTS(50).SAVE.10).F1(15).F2(15).F3(45)	· · · · · · · · · · · · · · · · · · ·
50		,
51	6 ANF, TON, FWS, RESTOZ	· · · · · · · · · · · · · · · · · · ·
52 C	SAVE OLD XDCT(41=49)	
53'	00 1C 1=40.49	- <u>-</u>
	10 SAVE((-39) - XUOT(1)	•
55 - C	·	· · · · · · · · · · · · · · · · · · ·
·56	00 25 I=1:17:2	•
•		to the frames

	-					
57		IF(T=wK(1)) 26,25,25				#
58	25	H=4K(I+1)	•		•	, , , , , , , , , , , , , , , , , , , ,
59	26	IF(w) 27.27.28				
- 60	27	PEX=0.0				
61		GO TO 29			•	•
62	28	PEX=1+0				
63	29	CONTINUE				
64	с		-OXYGEN	REQUIREMENT FUN	CT10N-V02MDT	
65		IF(002-LT-0-0)002=0-0	•			•
66		Vu2%0T=.0004850815*W/.25			•	
67		PSA==1.5+002				
. 68 .		DT1#002			* · ·	
69		DT2=(2.+D02-1.275)/1.15				
70		DT3#Dx+DL				
71		DT(N=SWIN(PSW.DT1.DT2)				
72		DT=FCNS*(PEX:DT3:DT3:DT1N)		AVVERD ABOT BI		m, mer r with the term of the grant and a second of
73 74	c	hatten and he a total	ALACIIC	OXYGEN DEBT DA		
75		DAIH=-15-(DT-1-5)+1-5				
76		- DAI#SHIN(PS/sDO2;DAIH) - DAO#FCNSH(PEX,O+O,G+G,DAI) = -				
77	•	T8=FCHS#(PEX:0.0.300.2.)				
78		XDaT(44)=(DAG=UA)/TB -				
79	c	XUU1111110AU-UA7718		OXYGEN DEBT DL		
		DL1H=-85+(0T+1.5)	LACITO	OXIGEN DEBI DE		/- #
81		DLI=Smin(PS#,0.0,DL1H)			· ·	· · · · · · · · · · · · · · · · · · ·
82		-DLO#FCN54(PEA,0.0,0.0,DL1)				*** -* ****
a 3		T7=FCNS+(PEX+0+0+300+.10+)				
84	··	XDOT(45)=(DLO-DL)/T8				
85	c		ARTERIA	L-VENOUS DXYGEN	DIFFERENCE AVD	
36		NUMPDI# . 038 + 002			•	e arm on a superior of the superior
87		CALL DELAYIO.0.05.NUMODI.AVD	T5, NUMPD	,1)		
88		AYD#Y020UT/CU		· · · · · · · · · · · · · · · · · · ·		
89		*5/1(96)Y-C6110N; = (94) 10CY				
90		IF(PEX.EU.D.D)FLAG=D.n	-			
91	•	IF (FLAG.EW. 1.0) GU TO 60				•
92		IF(PEX)60,60,61		• • • •	* * ****	
93		ANF=1.0		,		•
• •		-TDN=T+20.				
95 96	60	FLAG=1.0 IF(T.GT.TOH)ANF=0.0				
97	60	TAN=FCNS(ANF.3.+36+,3+)	•		, , ,	,
98		XDOT(49)=(11.00*ANF-XN3)/TAN	_		·	
99		ADOT(43)=(5.5.PEX-XN4)/6.				
		-DMMX=2+0				
101		DH=002+25+/22.				
102		IF (PEX+GT+0+0)DTS=DT				
103		IF (PEX.GT.O.D)ONS=DM				
184		IF (PEX-LT-1-10m=UMS/DTS+DT			,	
105		CHEMON#002/0.8				
186		IF (CHEMO: .GT . O .S) CHEMON#O.S		M 4 1447 W		
107		FN=2.+XN9+X93				
, 10a		- IF (FN+GT+11+) FN=11+		'		
109		IFIPEX.GT.O.IFNS#FH				_
110-		IF (PEX.LT.1.) FN=F4S/DTS+DT		,	••	
111	C	CONTROLLED RESISTANT	CES			· ω
	C	-LEGS		•	* ** ···	· · · · · · · · · · · · · · · · · · ·
4 113		RMET#150 ACCMET = 50 .		<i>,</i> ,		
					10000	

```
114
                     IF (RMET-LT. 15.) RMET=15.
                     RDM=450.-450.-DH/DMHX
    -115
    116
                     IF (RDM+LT+15+)RUH=15+
-----117----
                     REGCAP= (RMET+ROM)/1337.
                     REGARMORMET+ROM
    118
                     RLGARN=-FN+5400-/11.
  ~ 119
    120
                     RLGAR# (RLGARN+RLGARN+R400.)/1332. +RVACT
   - 121
                    OTHER BRANCHES
    122
                    RHCAP=3570./1332.
   - 123
                - - RCOR#(20500.-9395.*OM/DMMX)/1332.
    124
                    RSK8#(7640++6000++DL)/1332+
-- - 125
                    RRALE = (5000 . + 1600 . + 0L) /1332 .
    126
                    XMMG\ru=SMGP
    127
                    IF (RUMR - GT - 1 - ) RUMA = 1 -
    128
                    RC5NA=(5000++1070++(FH/11+/2++RDMR/2+))/1332++RVACT
    129
                    SUM#04
    130
                    UO 92 I=1.14
  -- 131
                    ·F1(I)=F1(I+1).
    132
                 92 SUM#F1(1)+SUM
- --133
              134
                    COT= (SUM+CO) / 15 .
   135
                    IF (COT . GT . 25 . ) CGT = 25 .
    136
                    RPA=+0175-+0075/21+ + COT
 -- 137
                    RPC=+0595=+0245/21+ + COT
    138
                    KPV≢RPA
   -139
                    RREFF + D.
                    IF (THETA-GT-15. -AND. T.GT-40.) GO TO 600
    140
    141
                    RC54A=(2490.+(4770.-4130.)=(FN/11./2.+6n/0MMX/2.11/1332.*RVACT
    142
                    RLGAN#(ADDD. -- 600. +PEA+RLGARN+RLGARM)/1332. +RVACT
    143
                    KRALE=(3600++(8020++5)40+)+DL/C+9)/1332+
    144
                AUD CONTINUE
                  - 5F=+67+.374+(X(40)=+9)
    146
                     IF (SF . GT . 1 . 135) SF=1 . 135+ . 46 = (X(40) = 2 . 143)
                    XDOT(40)=(V0200T=X(40))/T7
  - 147
                    1F(SF.LT.C.67)SF#+67
    148
-- -- -149
                    IF (5F.GT.3.) SF=3.
    150
                    IF (PEX.LT.1. .AND. THETA.LT.45.) SF#.48
  -- 151-
                 -- - IF (THETA - GT - 15 - - AND - T - L T - 40 - ) SF = - 48
    152
                    SF=SF+PD(11)
-- . 153 -- -
          ---- 610 CONTINUE.
    154
                                                    PRESSURE REFERENCE FUNCTION PR
              C
   155
                    PRN#86.+C1.DU2+C2#ACCMET
    156
                    EH=PRN=PH/2.=PMC/2.+XN3+3.*XN4+FN/2.
-- 157 --
                    SuH=G.
    158
                    00 91 1=1+14
--- 159
                    F2(1)#F2(1+1)
    160
                 91 SUM#F2(1)+SUM
                    F2(15) = EN
--- 161
    162
                    EF=(SUM+EN)/15.
 --- 163
                    PAVG=PO(1)
    164
                    IF (PAVG.LT.95. .AND. PAVG.GT.69.) GAIN#
                   6 (4.1-3.77/6.*(PAVG-49.))*64EW
    165
    166
                    IF (PAVG.LE. 59.) GAIN=4.1. GREW
                . - IF (PAVG.GT.95.) GAILH.33.65.EA
    167
    168
                    IF (PEX. GT. D. ) GAINE, JJ. GNE.
   169
              - - - .DDP=G.533+(ER+GA14)
    170
                    IF (DDP.LT.C.G)DDY=C.C
```

			• • • • • • • • • • • • • • • • • • • •
17:	TOT=0.300+DOP		
	- HR=60./TOT -	* * #= *	
173 C	CONTROLLED COMPLIANCES	1	•
- 174	· ERC=(PRN-PHC) 7 .	•	
175	SUX#0.		
176 177	00 90 1=1,44 F3(I)=F3(I+1)		
	-90 SUr=F3(1)+SUH	·	
179	F3(45)#ERC		
160 -	ERC#(SUM+ERC)/45.		and administration of the state
181	IF(ERC.LT.D.D)GO TO 7		
1 0 2 1 3 3	1F(EHC+GT+HO+)EFC=HO+ CLGVE=3+956+(1+0~+0083+ERC)	•	
184	CLGSV=3.1435*(1.00003*ERC)		
185	7 CONTINUE		
186 C	RESPIRATION *	-	a company with the same of the standard management of the same of
187	RESTG2=.313		•
168	- IF (THETA-GT-15. AND. T.GT-40.) RE	ST02*+37 - · · · · · · · · · · · · · · · · · ·	and the three reals a per the handparent of the salar and man and course
189 C	FREC=V0200T=8.24+5.28	•	
190 191	IF(FKEC.GT.30.)FREQ=3n TR=60./FREQ		•
192	" XDGT(41)={VG2DGF~C+38)++4/300+	, , , , , , , , , , , , , , , , , , , ,	
193	IF(PEX.EG.C.C)XGOT(41)==1./300+		
- " 194 -	T IF (ACCMETALE . D . D . AND . PEX. EC . D . C) XDO	T(41)=0.0	ښې پې و منده و سبت ف سبت پېټ دي ده مخبخت او مست
195 C	OXYGEN	DEFICIT FUNCTION DO2	
• 7 6	CALL DELAY(C.C.5. VOZDOT. VOZTS, VOZDD		West 20
197 198	%DOT(46)=(-vc2DL+PEX*vc2%DT+0.33)/6 if(DO2.LE.O.C.A%D.PEX.EG.O.G)%DOT(4		
199	00 31 I=40,49	87-040	
200	31 X(1)=X(1)+C.1+(XGGT(1)+SAVE(1+39))	A. C. Company	
201	RETURN		
202	END	A 1	* * * * * * * * * * * * * * * * * * * *

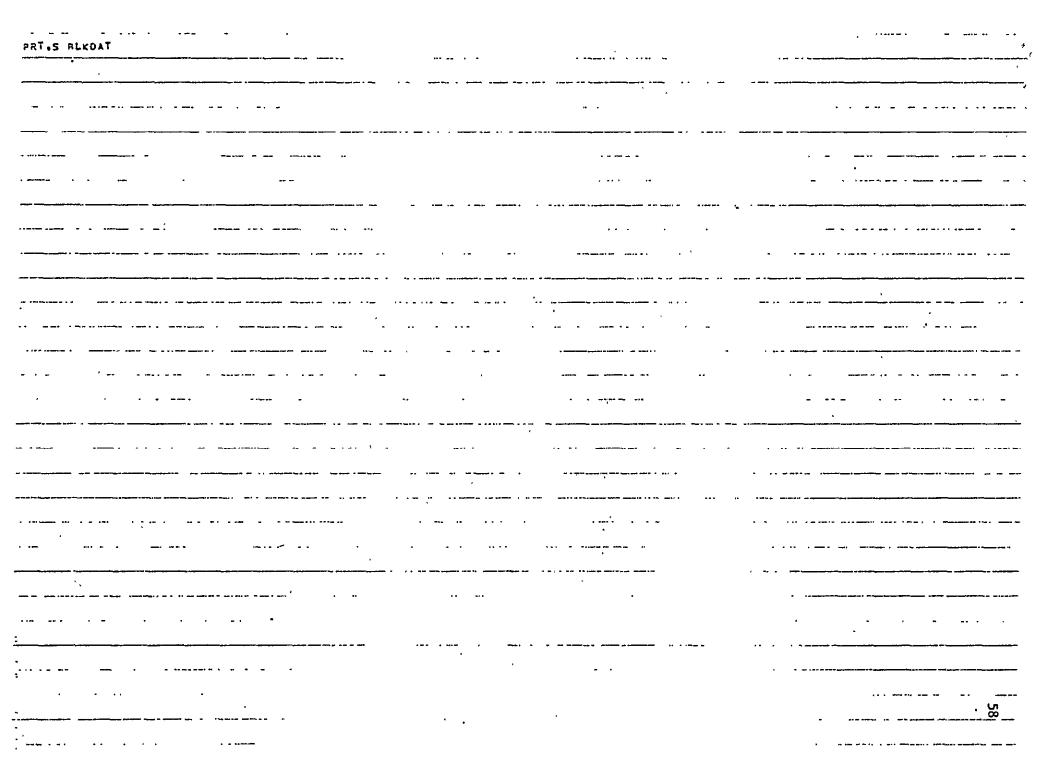
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SPRT.S ALGO		,) (**
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	•	<u>,</u>
D86-GD3432-TPF5-ALGO		
2 C INTEGRATION ALGORITHM		
3 COMMON /STATE/ X(SG), XDOT(50)		······································
4 % CIMENSION XDS(50) 5 - 00 3 1#1+34	•	
6 3 XDS(1) = XDOT(1)		/
7 ne0-001		
8 IF(T.GT.11.) H=+ CC2		
т т 9 Т≒Т+н		
10 CALL CVS 11 00 4 1=1.34		
12 4 x(1)=H/2. (xDOT(1)+xDs(1))+x(1)		
14 END		
•		Ma =
GPRT.S XIO	,	
	- -	
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DB6-GD343Z*TPFS*XIO		,
2 CONMON/STATE/X (6CD)	•	
3 COMMON/XIOD/N(9), NH(8), INIT, A(9,6)		
4 DATA KY.NWTL/IHN.6H TILT/		
· 5 7=x(598)		
6 IF (INIT-GT-0) GO TO 200		:
7 ~	,	· · · · · · · · · · · · · · · · · · ·
6 CALL CDATE (MD)		•
GALL CTIME(MT)		
' 10 hRITE(6,5)MD:MT		
. 11 5 FORMAT(/ CARDIUVASCULAR TILT ERGOMETRY MODEL . 6X		* ** ** * * * * * * * * * * * * * * *
12 • REFER TO GE-AGS USER GUIDE TIR 741-MED//		
14 X (495) = [
16 C 6 FORMAT (F5.0)		•
17 9 ORITE (0.10)+ -		
18 10 FORMAT(+ ODO YOU WISH TO CHANGE INITIALIZED DATA? (Y/	(N) *)	
19 KEAD (5,20) K	4 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
20 20 FORMAT(1A1)	·	- -
21 - 1F (K.EQ.KY) GO TO 60	·	
,22 ARÍTE (6,30)		
- 23 30 FORHAT(OPLEASE ENTER INDEX(1-600), VALUE, CR: (13,6	[12+6] *)	** * ** ** ** * * * * * * * * * * * * *
24 GO TO 4D		
25. 25. 25. 25. 25. 25. 25. 25. 25. 25.		
26 40 KEAU (5.5C.ERR#35) I, VALNEM	•	
27 50 FCRMAT(13.E12.6) 28 ARITE (6.55) 1.VALNEW		
7 29 7 55 FORMAT(4x,3H***,14,Fin,4) 30		
31 X(1) = VALNER		
· 32 GO TO 40		
33 60 ARITE (6.70)	,	
. 34 70 FORMAT (1000 YOU WISH TO MODIFY THE OUTPUT LIST? (Y/M	43 * 3	•
" 35		and the state of t
. 36 IF (K.EG.KY) GO TO 2GA	•	
37 WRITE (6,80)		
38 80 FORMAT (*GPLEASE ENTER POSITION(2-9), INDEX(1-600),	•	<i>'</i>
- 39 - 6 ! LABEL, CR: (1:,14.A6:)) 40 - 60 TO 90		A series of the
40 GO TO 90 41 AS 5x1TE (6.86)		
42 86 FORMAT (* •READ ERROR•*)		The second secon
43 90 READ (5,100,EPR*65) IP.1(N/B		
44 100 FORMAT([1:14:40)		, , , , , ,
45 #RITE (6,101) IP, I, NAR	***************************************	
46 IQ1 FORMAT(4X,3m+++12,14,1X,A6)		
47 IF (IP*E0*0) GO TO 200	*	
48 IF (IP.ED.1) GO TO 9	·	*

50 IF (1.LT.1 .UR. 1.GT.430) GO TO 85		,
51 Go To (93,102,103,104,105,106,107,108,109),1P		* · · · · · · · · · · · · · · · · · · ·
52 102 N(1)=I 53 NA(1)=NER *		
;53	• • •	
55 103 N(2)=1 · · ·		, Lm
56 K4(2)=NAB	,	,
1		

1		
'		•
57 GO TO 90 58		P .
58104 №(3}#1 59 NA(3}#N#B		·
61 105 N(4)=1	•	···
62 N#(4)=N#B		•
63 'GO TO 70		·
	•	
65 N#151=N#8		•
66 GO TG 9D		
67 107 N(6)=1 68 - N#(6)=N#B		
49 GO TO 90		•
108 N(7)*[
71 NA(7)=NAB		
72 - GO TO 9N		
73 109 N(a)*I		
74 NH(6)=NH8 +-		
75 60 TU 90		
76200 CONTINUE 77 IF (T.GT.D.CO1) GO TO 215	1040 4 900004 1900 10	- was a second day of the control of
78 1F (X(495)-LT-0-5) GO TO 210		
79 IF (N(7).NE.469) GO TO 210		***************************************
80 · · NA(7)=NATL	•	
81 N(7)=575		
52 210 mRITE (6.205) Nn.(N(I),I=1.6)		
83 205 FORMAT(///* SECS*,8(2x.46)/* 599*,618/* ****	• • •	
85 215 DO 220 (=1.9		
80 KWN(I)		
87 A(1,5)*X(K)		
88 220 A(1,6)=(A(1,1)+A(1,2)+A(1,3)+A(1,4)+A(1,5))/5.0		FA 1 (4 M
89 X(570)=A(Y,6)		
90 - · · IF (N(7) . EQ . 575 . AND . T.LT. +1.) A(7,6) *0.		س يو موسيه و خفيه بد ي س
91 C #RITE(6,300)T,(A(1,5),1=1,8)	• •	
92 IF ((T-PT)-LT-1-1 + OR. AMOU(T.ABS(X(599)))+GT-1+) 6	io TO 310	
93 LP=7		•
75 PRITE(6,300)PT,(A(I,6),Im1,6)		
- 96 "-300 FORMAT (F7-1-AFE-3)		
97 IF (A(599).GT.D.) GC TO 310	•	
98 DIMENSION NXP(24) RNXP(24)		· · · · · · · · · · · · · · · · · · ·
99 DATA NXP/45,48,564,491,571,124,123,134,138,150,121,		•
100 6 201,203,227,221,233,249,250,41,576,135,44,242,205/	•	~ ****
101 00 301 1=1,24		
102/ J=h;xP(1) 103 301 RNXP(1)=X(J)		
104 641TE (6,305) RNAP		
105 C ARITE (6,305) (X(I),1=1,32)		
107 310 Do 320 J±1.4		
108 00 320 I=1.9 ··		** * * * ** ** ** ** ** ***
109 320 A(1,J) = A(1,J+1)		
110 - KETURN		*.
111 END		<u>,</u> (τ, ·
		···



086~603432*TPFS*8LKDAT		•
		<u> </u>
2. COMMON/STATE/A(100)		
3···· COMMON/STATE/8(50)		
The state of the s		· · · · · · · · · · · · · · · · · · ·
4 COMMON/STATE/C(50)		•
5 · · · · COMMON/STATE/D(50),		7 M 9 mm or 4 10mm on 11 mm on
6 COMMON/STATE/E(50)		
7: COMMON/STATE/F(20)		· · · · · · · · · · · · · · · · · · ·
8 COMMON/STATE/G(28D)		
7 9 Cee STATE		
10 DATA A/89.9,215.8,38.7,213.0,7.7.10.6,27.4,6.5,0.,0.,	1- 10	
the state of the s	11 ~ 2n	
**		
12 2 355+2+253+5+36+4+23+5+31+2+63+4+3+1+254+2+3+2+120+7+	21- 30	
13 3 17*1:43*7:5*0*10*0*17*0*:50*0*/	31-100	
14 C++ FLOW -	•	V
- · 15 - DATA 8/39*0.,204.,204.,206.,211.,212.,214.,215.,231.,0.,0.,0.,0.	101-150	<u></u>
16 Cee COMP		
17 DATA C/4+0i.2.1.7,5.325,2*02*.2.021,.2,.8,.3,3.96,3.14,	151-17n	
18 1 3 0 0 1 2 3 9 7 6 1 5 - 3 1 - 5 9 5 5 7 , 1 - 5 9 5 , 6 - 0 4 7 ,	171-18C	
	181-200	
- · · · · · · · · · · · · · · · · · · ·	181-200	
20 C++ PRES		
21 DATA D/48+D.:0.001:7+n.,2+90./	261-250	
. 22 C. RES		
23 - UATA E/3**907506,*004.*01592,*05255,*015022,2*0*,*01200,	251-260	
24 1 .0400,00340000034003003,4.505,.4505,.07508,.07508,.02102	261-270	•
25 	271-280	
26 3 .34.534522525255300301502,.45045,2.744,.6494,00	281-290	•
27 == 4 9.0.,5,15/	291-360	
28 Cee Inst	411-200	
- 29 DATA F/.GDD7508602.7.004004.004.000400626.11.00./	301-320	
	AOT SEC	***************************************
30 C++ M15C	221-165	
31 DATA G/48*0+5500++5500++30++0++30++6++15++400++61+6+2*0++		· · · · · · · · · · · · · · · · · · ·
32 1 0 • • 90 • 5 • 0 • • 43 • 5 • 5 • 1 9 4 • 30 • • 1 30 • • 1 38 • • 40 • •	381-390	•
	391-400	
34 3 50 • 150 • 18 • 0 • •	401-420	
35 34*D+.32*Q4*D882.55:3.60.79990	421-495	
36 • 0 • 10 • 0 • 6 • 6 • 6 • 7 • 0 • • 7 • 0 • • • 2 • 0 • •	496-510	•
37 4 3[0.,[0.,[6.,6.,[0.,2.n.,]6.,14.,	. 511-520	
38 5 140,20,-70,-140,00,00140,13000	521-540	** ,
4 39 + D., C., 160., 600., 400., D., 131., 401.,	541-540	•
	· · · · -	
40 6 72.,.09,6.7,5.0.,8.3,0	561-570	•
417 •D550.01.5.070486331936.46	571-580	** ** * ** ** ** * * * * * * * * * * * *
42 8 10 • 1 ~ • 0 15 • 85 • • 14 ~ € • • • • 0 • 10 • • 0 • /	581-600	
43 COMMON/XIGD/N(9), halls, init	•	· · · · · · · · · · · · · · · · · · ·
. 44 OATA INIT/O/		ı
45 DATA NAZ' HR', T CO', T SV', TVO2DOT',		, , , , , , , , , , , , , , , , , , , ,
46 F SYSTE DIASPER TILT . LEGY!		
47 DATA N/561.563.562.570.567.568.575.600.570/		
48 COMMON/RINTR/RIN(10) ROUT(10)		
SO END	•	•
30 GNV		
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	RC6(D).		
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	RCB(O)		
REL			
FOR	86910}		
REL	RC9		
FOR	RC10(0)		
REL	RC10		
FOR	RC11(0)	**************************************	
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	RC15(0)		
	RC15		
FOR	RC16(0)		
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	RC17(0)		
REL	RC17		
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	RC20(01		
	RC20		
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REL For	RCF1(0)		
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FOR	RC13/SIMP(0)			•
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ELT	RUNEX(O)			
ELT	RUHOL(0)		- 1	
FLT	RV6(0)			•
FOR	ALGO(0)			
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FOR	CONTRE/OL(O)			
FOR	CVS/04(0)			
FOR	6K001N/0L(0)		•	•
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8. BIBLIOGRAPHY

- 1. Guyton, A. C., et al., Circulation: overall view, Annual Review of Physiology, Vol. 34, pp. 13-46, 1972.
- Gallagher, R. R., Investigations of respiratory control system simulations, Final Research Report, General Electric Company TIR 741-MED-3046, Houston, Texas, 1973.
- Stolwijk, J.A.J., A mathematical model of physiological temperature regulation in man, NASA Report NAS 9-9531, 1970.
- 4. -Croston, R. C. and D. G. Fitzjerrell, Cardiovascular model for the simulation of exercise, lower body negative pressure, and tilt experiments, Fifth Annual Pittsburgh Conference on Modeling and Simulation, April, 1974.
- 5. Gallagher, R. R., Evaluation of exercise-respiratory system modifications and integration schemes for physiological systems, Final Research Report, General Electric Company TIR 741-MED-4018, Houston, Texas, June, 1974.
- 6. Marks, V. J., User's instructions for the Grodins' respiratory control model using the Univac 1110 remote batch and demand processing, General Electric Company TIR 741-MED-4024, Houston, Texas, September, 1974.
- 7. Archer, G. T., User's instructions for the Grodins' respiratory control model using the Univac 1106/1110 batch and demand processing, General Electric Company TIR 741-MED-3055, Houston, Texas, October, 1973.